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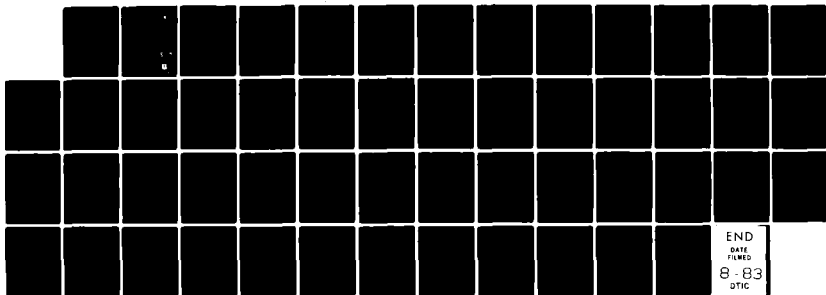
AN EVALUATION OF AN AUTOMATIC CELL DETECTION AND
TRACKING ALGORITHM(U) AIR FORCE GEOPHYSICS LAB HANSCOM
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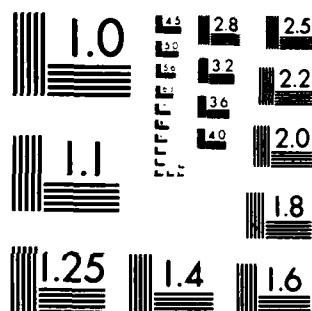
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An Evaluation of an Automatic Cell Detection and Tracking Algorithm

JAMES G. WIELER
F. IAN HARRIS
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3 November 1982

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METEOROLOGY DIVISION
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PROJECT 2781

AIR FORCE SYSTEMS COMMAND, USAF



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| 20. ABSTRACT (Continue on reverse side if necessary and identify by block number) A storm tracking algorithm designed to detect and track fine structure in digitized radar data is evaluated. These fine structures are defined by regions containing values within 3 dB of peaks in reflectivity factor. The algorithm describes storm structure and evolution by correlating these peak regions in time and space. The evaluation consists of a comparison of the algorithm output with raw data and with output from an AFGL algorithm which detects and tracks three-dimensional reflectivity weighted centroids defined by a preselected threshold. | | |

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It is concluded that the algorithm cannot reliably detect and track significant structures within storms when applied to data sets with a temporal resolution of ~6 min and a spatial resolution of 1.0° in azimuth and 0.7° in elevation. The significance of tracking 3 dB peaks is questioned and the implication of defining a larger peak threshold is discussed. The algorithm does track the large features of storms with results similar to the AFGL algorithm. However, it does not run in real time and is not modular, unlike the AFGL algorithm.

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An Evaluation of an Automatic Cell Detection and Tracking Algorithm

I. INTRODUCTION

The large amount of data available from Doppler weather radar systems (for example, reflectivity, radial velocity, and velocity variance fields) make it nearly impossible for an operational forecaster to observe, interpret, and integrate all the data into a forecast product. Many of the algorithms developed for the NEXRAD software package will automate the analysis of Doppler weather radar data in real time and provide useful, easy to interpret products for the operational meteorologist.

As the Technical Evaluation Facility (TEF) for the NEXRAD project, the Air Force Geophysics Laboratory's (AFGL) Ground Based Remote Sensing Branch is developing and evaluating proposed algorithms for the NEXRAD system. In this report we present an evaluation of the Automatic Cell Detection and Tracking Algorithm proposed and developed by Crane^{1,2,3,4,5} and Gustafson and Crane,^{6,7} as an operational tool.

(Received for publication 3 November 1982)

The Next Generation Weather Radar (NEXRAD) is a joint agency program to develop and acquire a surveillance Doppler weather radar system for the Departments of Commerce (DOC), Defense (DOD), and Transportation (DOT). The NEXRAD system will replace aging DOC and DOD weather radars, and improve severe weather detection capabilities.

(Due to the large number of references cited above, they will not be listed here. See References, page 29.)

We have based the evaluation on an analysis of the timing, accuracy, and limitations of the algorithm assuming:

- a 5-6 min elevation angle sequence (volume scan) repeat time;
- and
- products will be useful to at least a range of 230 km.

The analysis consists of checks of the algorithm products against both raw data and output from the Automated Real-Time Storm Analysis and Storm Tracking (WEATRK) developed by Bjerkaas and Forsyth.⁸

All the data used in this analysis were archived during the 1979 Joint Doppler Operational Project (JDOP) (Donaldson and Glover⁹) by AFGL's 5-cm radar located at the Doppler Radar Facility of the National Severe Storms Laboratory near Norman, Oklahoma.

2. THE AUTOMATIC CELL DETECTION AND TRACKING ALGORITHM

2.1 Algorithm Overview

The Automatic Cell Detection and Tracking Algorithm (ACDT) was designed to detect and track certain features of precipitation echoes observed in weather radar data. These features are:

- 3 dB peaks defined by contours of reflectivity 3 dBZ below individual peaks in the reflectivity field,
- Volume cells consisting of vertically correlated 3 dB peaks,
- Contour regions defined by one fixed reflectivity value (for example, 30 dBZ) at the lowest available elevation angle,
- Clusters defined as groups of volume cells within a single contour, and with spacings less than some minimum distance.

2.2 Storm Attributes

The following is a discussion of the various attributes which are computed for each of the features listed above.

8. Bjerkaas, C.J., and Forsyth, D.E. (1980) An Automated Real-Time Storm Analysis and Storm Tracking Program (WEATRK), AFGL-TR-80-0316, AD A100236.

9. Donaldson, R.J., Jr., and Glover, K.M. (1980) Joint Agency Doppler Technology Tests, AFGL-TR-80-0357, AD A100208.

2.2.1 3 dB PEAKS AND VOLUME CELLS

3 dB peaks are characterized by the attributes listed in Table 1.

These peaks are detected and attributes, compiled and stored for each elevation angle. After a volume scan* is completed the 3 dB peaks are vertically correlated to build three-dimensional structures called volume cells.

The algorithm produces a hierarchy of volume cell types, removes false volume cells, and identifies significant volume cells. Significant cells are characterized as having a high degree of vertical continuity or having high reflectivity and some vertical continuity. Specifically these criteria for significance are:

(1) detection on more than 50% of all azimuth scans in a volume scan and more than 70% of the scans below 6 km; or (2) average reflectivity greater than 40 dBZ in more than 30% of the azimuth scans in a volume scan, with some portion below 6 km.

According to Crane,⁴ several types of volume cells are evident in the output from this algorithm. These are large mature (significant) cells, young growing cells, and ground clutter which is typically identified by cells that do not move and are close to the surface.

2.2.2 CONTOURS

Since contours are defined as regions enclosed by a preselected reflectivity threshold, they may encompass more than one volume cell. The attributes tallied for each contour region are listed in Table 1.

The motions of the volume cells enclosed by a contour are used to establish tracks for the contour regions, and to provide a directory for the mergers and splits of the contour regions. Estimates of liquid water flux averaged over the area of a fixed contour are useful for a relative evaluation of the contoured regions. The algorithm computes the total water mass flux rates only for observations at the lowest elevation angle to avoid contamination by ice.

2.2.3 CLUSTERS

Closely spaced volume cells are associated as belonging to a cluster, each cluster is tracked and attributes are compiled describing its structure and behavior. The cluster attributes are listed in Table 1. Crane and Hardy¹⁰ state that, at short ranges where the radar beam is sufficiently narrow to resolve the volume cells in a cluster, the cluster will represent active convection. However, at longer ranges, the volume cells in a cluster may not be resolved, in which case the convective element will be detected as a significant cell.

*A complete elevation angle sequence from lowest to highest elevation is called a volume scan.

10. Crane, R.K., and Hardy, K.R. (1980) The Hiplex Program in Colby-Goodland Kansas: 1976-1980, Final Report, Document P1552-F. Environmental Research & Technology, Inc., Concord, Massachusetts.

Table 1. List of Attributes Compiled From the Automatic Cell Detection and Tracking Algorithm (after Crane⁴)

| Function | 3 dB Peak | Volume Cell | Cluster | Fixed Contour | Volume Scan Summary |
|-----------|---|--|--|---|--|
| Intensity | <ul style="list-style-type: none"> • Avg. Reflectivity | <ul style="list-style-type: none"> • Avg. Reflectivity • Reflectivity at Lowest Ht. • Reflectivity at summit • Peak reflectivity | <ul style="list-style-type: none"> • Avg. Reflectivity • Peak Reflectivity | <ul style="list-style-type: none"> • Avg. Reflectivity • Peak Reflectivity | |
| | <ul style="list-style-type: none"> • Avg. Tangential Shear | <ul style="list-style-type: none"> • Avg. Tangential Shear • Peak Tangential Shear | <ul style="list-style-type: none"> • Avg. Tangential Shear • Peak Tangential Shear | | |
| Location | <ul style="list-style-type: none"> • Centroid Position | <ul style="list-style-type: none"> • Centroid Position | <ul style="list-style-type: none"> • Centroid Position | <ul style="list-style-type: none"> • Water Flux • Reflectivity Centroid • V. Cell Centroid[*] • Sig. Cell Centroid | <ul style="list-style-type: none"> • Water Flux |
| Motion | | <ul style="list-style-type: none"> • Velocity of Centroid | <ul style="list-style-type: none"> • Velocity of Centroid • Velocity of V. Cells | <ul style="list-style-type: none"> • Velocity of Centroid • Velocity of V. Cells • Velocity of Sig. Cells | |
| Size | <ul style="list-style-type: none"> • Area | <ul style="list-style-type: none"> • Area at Lowest Ht. • Area at Peak Volume | | <ul style="list-style-type: none"> • Area | <ul style="list-style-type: none"> • Area |
| Height | <ul style="list-style-type: none"> • Elevation Angle | <ul style="list-style-type: none"> • Lowest Height • Height Base • Height Peak • Height Top • Height Summit | <ul style="list-style-type: none"> • Highest Summit Height | <ul style="list-style-type: none"> • Highest Summit Height • Avg. Height First Echoes | |

Table 1. List of Attributes Computed From the Automatic Cell Detector and the Sample-Abscissa-Intercept (C-m²) (Contd)

| Function | 3 dB Peak | Volume Cell | Cluster | Fixed Contour | Volume Scan Summary |
|-----------|--|---|---|--|--|
| Star-type | <ul style="list-style-type: none"> • Contour Identity | <ul style="list-style-type: none"> • Contour Identity • Cluster Identity • Spread of Cell • Centroids | <ul style="list-style-type: none"> • Contour Identity • Spread of V. Cell Centroids • Correlation of V. Cell Centroids • Orientation of V. Cell Centroids† • No. of V. Cells | <ul style="list-style-type: none"> • Complex Identity • No. of V. Cells • No. of Clusters • No. of Sig. Cells and Clusters • Spread of V. Cells • Spread of Clusters • Spread of Sig. Cells • Orientation of V. Cells • Orientation of Clusters • Orientation of Sig. Cells • Correlation of V. Cells • Correlation of Clusters • Correlation of Sig. Cells | <ul style="list-style-type: none"> • No. of Contours • No. of V. Cells • No. of Sig. Cells and Clusters |

*V. Cells are Volume Cells

Sig. Cells are Significant Cells

†Correlation of X location (east) vs Y location (north)

3. AN AUTOMATED REAL-TIME STORM ANALYSIS AND STORM TRACKING PROGRAM (WEATRK)

3.1 Algorithm Overview

The following is an abbreviated description of the Automated Real Time Storm Analysis and Storm Tracking Program (WEATRK).

The WEATRK algorithm defines a storm cell as any region contained within a predetermined reflectivity contour. The storm attributes tabulated by this algorithm include:

- Storm volume,
- Storm mass,
- Mass-weighted centroid,
- Maximum reflectivity and its height,
- Maximum radial velocity at the lowest elevation angle, and
- Maximum spectral variance and its height.

Radar data for this algorithm is acquired via a series of azimuth scans over a volume scan. Reflectivity segments along each radial exceeding a predetermined threshold are identified and correlated azimuthally to define two-dimensional storm cells. After the completion of a volume scan the storm cells are correlated in the vertical to define a three-dimensional storm. Any single level feature that is not correlated with any other in the vertical is removed from consideration. The volume centroid is then computed in three dimensions using a mass-weighted algorithm. The maximum reflectivity and height are computed using a three-dimensional squares fit technique to the reflectivity data.

4. CASE STUDIES

The first case study was a severe weather event that occurred on 12 April 1984 in the central United States. The event was characterized by a strong low-level jet, a deepening surface low, and a rapidly intensifying storm system. The WEATRK algorithm was applied to the radar data from this event, and the results were compared with those from the ACDF.

The second case study was a severe weather event that occurred on 15 May 1984 in the central United States. The event was characterized by a strong low-level jet, a deepening surface low, and a rapidly intensifying storm system. The WEATRK algorithm was applied to the radar data from this event, and the results were compared with those from the ACDF.

4.1 Case Study No. 1

The first case study consists of four volume scans recorded between 1555 and 1621 CST on 2 May 1979. These four volume scans are a subset of an eleven volume scan run of the algorithm, and are assessed to be representative of the algorithm's behavior.

The data, for this case, reveals two well-defined storms northwest of the radar (ranges from 120 to 200 km). A cursory glance at Figures 1, 2, 3, and 4 reveals some internal structure in each. The centroid locations of the ACDT contour regions (numbered) and those of the WRAFRD storm cells (lettered) are marked on each plot.

Output from the ACDT for Case Study No. 1 can be seen in Tables 2, 3, 4, and 5. The output consists of five parts:

- (1) Volume Scan Header Information,
- (2) Fixed Contour Header Attributes,
- (3) Contour Cell Attributes,
- (4) Cluster Attributes, and
- (5) Volume Scan Summary.

The attributes for parts 2-5 are listed in Table 1. For a more comprehensive discussion of these attributes and their derivation, see Gustafson and Crane.⁷

From the fixed contour output of Table 2 it can be seen that the ACDT has identified two storms (1 and 2) at the lowest elevation angle (0.4°) along with one other very small feature (3) 217 km from the radar. Six minutes later (Table 3) these same three contours are found along with a new one (4) which is identified as a split from 1 (last column on right). However, with the next sequence (Table 4) the algorithm has declared that contour 4 has merged back with 1 (second to last column on right), and has identified a new cell (5) at a range of 203 km. In the last sequence to be presented here we see that 2 has merged with 1 (Table 5 and Figure 4) and 6 has split from 3.

Although some of the merging and splitting may seem a little artificial (that is, contour region 1 and 4), it is a function of the threshold (30 dBz) used to define the contour regions and the perturbations around that value. Contour region 4 is not readily apparent in Figure 2 due to the smoothing in our contouring routine. It is, however, apparent in the raw data, where two adjacent range gates with reflectivities of 28 and 29 dBz separate two areas of reflectivity greater than 30 dBz. The contoured region between contour regions 1 and 2 (marked x in Figure 1) does not contain a 3 dB peak and is therefore not listed by the algorithm.

CONTOURS OF DBZ

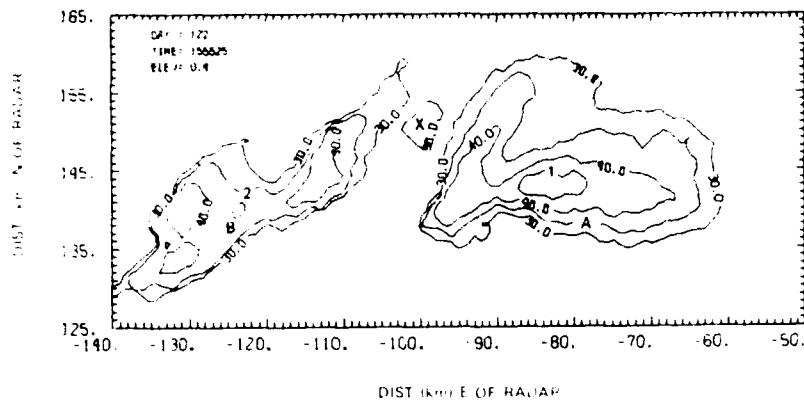


Figure 1. Reflectivity Contour Plot for Volume Scan Beginning at 1555

CONTOURS OF DBZ

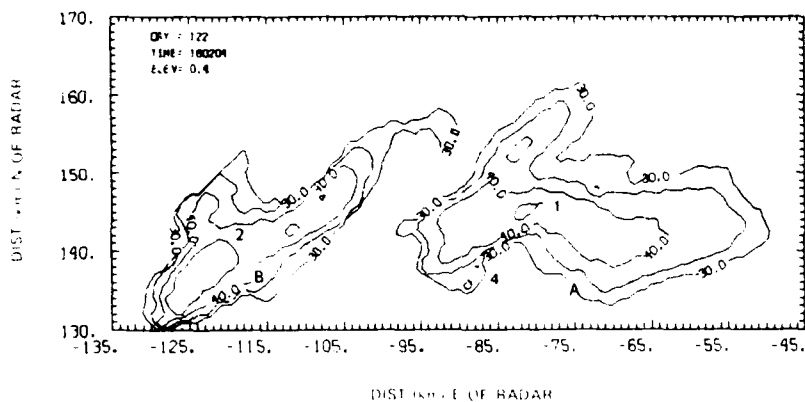


Figure 2. Reflectivity Contour Plot for Volume Scan Beginning at 1601

The contour region centroid locations are determined by averaging the centroid locations of the volume cells enclosed by the contour region. The contour region centroids appear to be located in the correct positions judging from the concurrent lowest elevation contour maps. The peak reflectivities enclosed by the contour regions, and the contour region's speed and direction seem to be reasonable within the resolution of our analysis.

CONTOURS OF DBZ

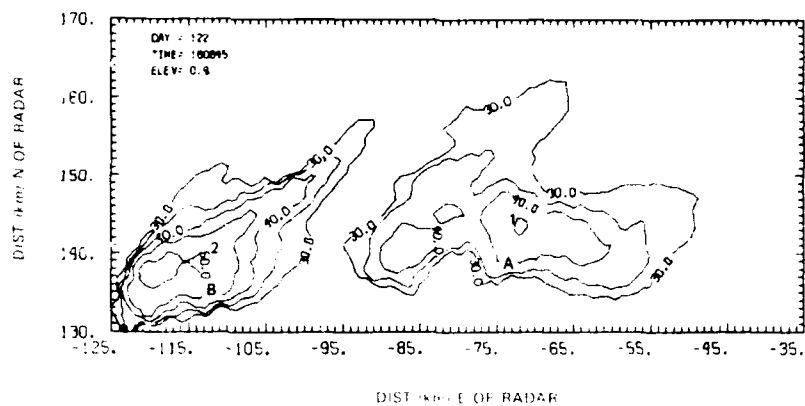


Figure 3. Reflectivity Contour Plot for Volume Scan Beginning at 1000.

CONTOURS OF DBZ

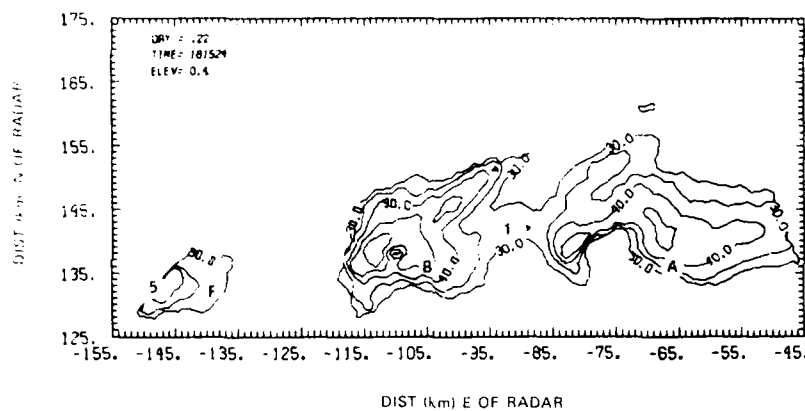


Figure 4. Reflectivity Contour Plot for Volume Scan Beginning at 1015.

4.1.1 ACDT-WEATRK PRODUCT COMPARISON

The output statistics for WEATRK storm cells identified in the four volume scans of this case study, and the closest corresponding contour regions from the ACDT are presented in Table 6. The same threshold value was used for determining the WEATRK storm cells and the ACDT contour regions.

Table 2. ACD1 Volume Scan Output for Volume Scan No. 1

SCAN TIME 122 155507 - 160107 VOL SCAN 1: A2 -137.1 TO 119.8 (DEG)
 TRACK REF TIME 1555 7 - 155507 AZM SCAN 10/C EL - 0.4 TO 6.5 (DEG)

NFA = 10, NVMA = 18

FIXED CONTOUR OUTPUT

| CENTROID | | AV | CELL | Z | N | N | K | SPR | SPR | C | WTR | AREA | VELOCITY | NEAR | MX | PR | SP | | | |
|----------|-----|-----|------|-----|----|----|---|-----|-----|-----|--------|------|----------|------|-----|------|------|----|----|----|
| TRK | AZM | RNG | AZM | RNG | AV | PK | V | S | C | X | L | R | FLUX | XSCN | AV | CELL | CIST | HT | ID | ID |
| NO | DEG | KM | DEG | KM | DB | DB | C | C | L | KM | KM | T | M/M | K/M2 | DEG | M/S | KM | KM | NO | NO |
| 1 | 330 | 167 | 329 | 164 | 42 | 47 | 6 | 2 | 1 | 3.4 | 9.6290 | 4.77 | 0.61 | 999 | 999 | 6.9 | 12 | C | C | |
| 2 | 319 | 188 | 320 | 188 | 43 | 46 | 4 | 2 | 1 | 3.0 | 9.2 | 62 | 2.54 | 0.37 | 999 | 999 | 0.0 | 10 | C | 0 |
| 3 | 329 | 217 | 329 | 217 | 44 | 44 | 1 | 0 | 0 | 0.0 | 0.0 | C | 0.61 | 0.08 | 999 | 999 | 0.0 | 6 | C | 0 |

VOLUME CELL OUTPUT

| CENTROID | | - | Z | - | HGT | VBAR | CELL | SPACIAL | (TAN) | CCP | RAC | RAC | CS | CK | D | R | | | | | | |
|----------|------|-----|----|----|-----|------|------|---------|-------|------|------|------|------|-------|-------|-------|-----|----|----|---|---|---|
| TRK | FST | NDR | AV | PK | LW | HI | L | M | H | EM/S | AM/S | SPRD | A | (SHR) | SPD | VEL | SPC | TR | TR | C | E | E |
| NO | KM | KM | DB | DB | DB | DB | W | N | I | CLD | ID | KM | KM2 | (PSK) | PSK | M/S | M/S | NO | NO | P | P | J |
| 1 | -131 | 142 | 42 | 43 | 43 | 5 | 5 | 5 | 11.8 | 2.1 | 0.00 | 9.2 | 1.4 | 0.0 | -9.5 | 4.6 | 0 | 2 | 1 | 1 | 1 | |
| 2 | -128 | 136 | 39 | 43 | 40 | 32 | 4 | 610 | 11.8 | 2.1 | 0.78 | 16.7 | 3.4 | 0.0 | 0.2 | 1.0 | 0 | 2 | 7 | 4 | 1 | |
| 3 | -114 | 143 | 46 | 46 | 46 | 4 | 4 | 4 | 11.8 | 2.1 | 0.00 | 3.5 | 1.7 | 0.0 | -9.1 | 3.3 | 0 | 2 | 2 | 1 | 1 | |
| 5 | -112 | 148 | 41 | 44 | 44 | 36 | 4 | 5 | 11.8 | 2.1 | 0.00 | 7.7 | 0.0 | 0.0 | -14.0 | 0.3 | 1 | 2 | 0 | 2 | 1 | |
| 6 | -95 | 139 | 40 | 42 | 34 | 42 | 4 | 6 | 7 | 11.8 | 2.1 | 0.00 | 6.0 | 1.7 | 0.0 | -7.3 | 4.3 | 2 | 1 | 3 | 1 | |
| 7 | -99 | 143 | 43 | 44 | 44 | 42 | 4 | 4 | 5 | 11.8 | 2.1 | 0.00 | 8.1 | 0.0 | 0.0 | -14.0 | 0.7 | 2 | 1 | 0 | 2 | |
| 8 | -112 | 185 | 44 | 44 | 44 | 44 | 6 | 6 | 6 | 11.8 | 2.1 | 0.00 | 10.2 | 0.0 | 0.0 | -14.2 | 0.0 | 0 | 3 | 0 | 1 | |
| 9 | -83 | 149 | 43 | 47 | 47 | 37 | 4 | 4 | 7 | 11.8 | 2.1 | 0.00 | 18.3 | 2.0 | 0.0 | -8.9 | 3.9 | 0 | 1 | 7 | 3 | |
| 14 | -67 | 137 | 36 | 38 | 35 | 38 | 3 | 4 | 4 | 11.8 | 2.1 | 0.00 | 3.3 | 1.7 | 0.0 | -4.8 | 3.5 | 0 | 1 | 4 | 1 | |
| 15 | -80 | 137 | 44 | 44 | 44 | 44 | 5 | 5 | 5 | 11.8 | 2.1 | 0.00 | 11.5 | 2.3 | 0.0 | -2.7 | 4.4 | 0 | 1 | 3 | 1 | |
| 17 | -89 | 137 | 42 | 45 | 45 | 31 | 5 | 712 | 11.8 | 2.1 | 1.43 | 9.2 | 1.7 | 0.0 | -5.4 | 6.9 | 2 | 1 | 5 | 5 | 1 | |

CLUSTER OUTPUT

| CENTROID | | Z | N | SPR | SPR | ORT | CNT | VELOCITY | SPEAR | MX | PR | SP | CELL | CELL | NO | | | |
|----------|-----|-----|----|-----|-----|-----|-----|----------|-------|------|------|------|------|------|------|------|------|---|
| TRK | AZM | RNG | AV | PK | V | X | L | ANG | ID | AV | CELL | MSKM | HT | ID | ID | | | |
| NO | DEG | KM | DB | DB | C | KM | KM | DEG | EM/S | NM/S | KM | NO | NO | PSKM | MSKM | CS | | |
| 1 | 323 | 186 | 41 | 44 | 1 | 0.0 | 0.0 | C | 2 | 0.0 | 0.0 | 0.0 | 6 | C | C | 0.00 | 0.00 | 0 |
| 2 | 326 | 169 | 42 | 45 | 3 | 1.4 | 3.6 | 316 | 1 | 0.0 | 0.0 | 1.0 | 12 | C | 0 | 0.00 | 0.00 | 0 |

| VOL | NNM | AREA | WFLUX | NEAR | NEIGHBOR | ACT | NO | NO | VELOCITY | TRK | CLS | CNT | C | CVER |
|------|------|-------|-------|------|----------|-----|----|----|----------|------|-----|-----|-----|------|
| SCAN | K/M2 | KNT/H | CELL | CLST | CONT | VCL | CS | FC | EM/S | NM/S | NO | CTR | CTR | C |
| 1 | 1999 | 1.2 | 10.18 | 9.4 | 0.0 | 0.0 | 11 | 4 | 3 | 11.8 | 2.1 | 18 | 2 | 3 |

Table 3. ACDD Volume Scan Output for Volume Scan No. 2

SCAN TIME 122-160149 - 160745 VOL SCAN 2 #2 -169.23 TO 160.77 (DEG)
 TRACK REF TIME 16 1 2 - 160149 21# SCAN 10/0 EL - 0.4 TO 6.3 (121)

NFA = 10, NVMX = 21

FIXED CONTOUR OUTPUT

| CENTROID | | AV | CELL | 2 | N | N | N | SPR | SPR | 0 | WTR | AREA | VELOCITY | NEAR | MX | MR | SP | | | |
|----------|-----|-----|------|-----|----|----|---|-----|-----|-----|-----|------|----------|------|-----|------|------|----|----|----|
| TRK | AZM | RNG | AZM | RNG | AV | FA | V | S | C | X | L | R | FLUX | ASCA | AV | CELL | DIST | HT | IC | IC |
| NO | DEG | KM | DEG | KM | DB | GB | C | C | C | KM | KM | F | MMH | MMH2 | DEG | M/S | KM | KM | NO | NO |
| 2 | 320 | 185 | 321 | 184 | 43 | 49 | 5 | 2 | 0 | 4.0 | 8.1 | 49 | 4.41 | 0.36 | 158 | 15 | 0.0 | 9 | 0 | 0 |
| 4 | 327 | 163 | 328 | 160 | 43 | 49 | 2 | 2 | 1 | 0.0 | 0.0 | 0 | 0.05 | 0.01 | 214 | 12 | 0.0 | 10 | 0 | 0 |
| 3 | 331 | 217 | 330 | 217 | 44 | 44 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.70 | 0.10 | 218 | 17 | 0.0 | 4 | 0 | 0 |
| 1 | 332 | 165 | 329 | 169 | 44 | 45 | 2 | 0 | 0 | 0.0 | 0.0 | 0 | 4.63 | 0.04 | 243 | 10 | 0.0 | 3 | 0 | 0 |

VOLUME CELL OUTPUT

| CENTROID | | - | - | 2 | - | HGT | VBAR | CELL | SPACIAL | (TAN) | CCP | RAC | RAC | CL | CL | R | F | | | | |
|----------|-----|-----|----|----|----|-----|------|------|---------|-------|------|----------|-----|-------|-------|-----|-----|----|----|---|---|
| TRK | EST | NDR | AV | PR | EW | MI | L | M | M | EM/S | NH/S | SPKD | # | (SMR) | SPD | VEL | SPE | TP | TR | C | C |
| NO | KM | KM | DB | DB | DB | DB | W | N | I | CLD | IC | KM | KM2 | (PSF) | MSK | M/S | M/S | NO | NO | F | F |
| 1 | 123 | 145 | 40 | 40 | 40 | 3 | 3 | 3 | 3 | 17.0 | 5.3 | 0.0011.4 | 0.0 | 0.0 | 13.0 | 0.0 | 0 | 2 | 0 | 1 | 2 |
| 2 | 123 | 137 | 46 | 49 | 49 | 38 | 3 | 5 | 9 | 12.8 | 2.3 | 5.0011.6 | 2.2 | 0.0 | -3.1 | 6.5 | 0 | 2 | 5 | 4 | 1 |
| 3 | 109 | 144 | 44 | 44 | 44 | 44 | 3 | 3 | 3 | 10.9 | 2.8 | 0.0019.4 | 2.0 | 0.0 | -3.2 | 3.0 | 0 | 2 | 4 | 1 | 2 |
| 5 | 106 | 148 | 42 | 45 | 45 | 34 | 3 | 4 | 7 | 13.6 | 0.8 | 0.007.7 | 1.2 | 0.0 | -9.2 | 5.4 | 0 | 2 | 1 | 2 | 2 |
| 6 | 87 | 135 | 43 | 49 | 36 | 34 | 2 | 5 | 10 | 17.4 | -5.4 | 0.6510.7 | 2.1 | 0.0 | -6.8 | 4.0 | 2 | 4 | 5 | 4 | 2 |
| 7 | 90 | 145 | 44 | 44 | 44 | 44 | 3 | 3 | 3 | 10.3 | 3.0 | 0.0010.1 | 1.5 | 0.0 | -9.7 | 3.2 | 0 | 1 | 1 | 1 | 1 |
| 8 | 107 | 189 | 44 | 44 | 44 | 44 | 4 | 4 | 4 | 13.2 | 0.1 | 0.005.0 | 0.0 | 0.0 | -13.5 | 6.0 | 0 | 3 | 0 | 1 | 2 |
| 9 | 82 | 145 | 45 | 45 | 45 | 45 | 2 | 2 | 2 | 7.6 | 3.4 | 0.0010.3 | 0.5 | 0.0 | -5.0 | 4.3 | 0 | 1 | 1 | 1 | 2 |
| 14 | 66 | 138 | 36 | 36 | 36 | 36 | 4 | 4 | 4 | 6.5 | 1.6 | 0.002.9 | 1.0 | 0.0 | -2.4 | 5.1 | 0 | -1 | 5 | 0 | 2 |
| 15 | 81 | 135 | 43 | 47 | 43 | 39 | 4 | 6 | 8 | 2.8 | -3.0 | 0.679.5 | 2.3 | 0.0 | -4.8 | 3.7 | 0 | -1 | 1 | 2 | 1 |
| 17 | 86 | 139 | 35 | 35 | 35 | 35 | 4 | 4 | 4 | 9.2 | 4.1 | 0.006.4 | 2.4 | 0.0 | -4.5 | 0.0 | 0 | -1 | 1 | 0 | 2 |
| 20 | 120 | 132 | 40 | 43 | 43 | 32 | 7 | 7 | 8 | 11.8 | 2.1 | 0.0011.6 | 2.2 | 0.0 | -2.3 | 7.4 | 0 | 2 | 2 | 0 | 1 |

CLUSTER OUTPUT

| CENTROID | | 2 | N | SFR | SPR | ORT | CNT | VELOCITY | SHEAR | MX | MR | SP | CELL | CELL | NO |
|----------|-----|-----|----|-----|-----|-----|-----|----------|-------|-----------|------|------|------|------|------|
| TRK | AZM | RNG | AV | PR | V | X | L | ANG | IC | AV | CELL | MSKM | HT | IC | IC |
| NO | DEG | KM | DB | GB | C | KM | KM | DEG | EM/S | NH/S | KM | NO | NO | MSKM | HT |
| 2 | 327 | 161 | 43 | 49 | 1 | 0.0 | 0.0 | 0 | 4 | 21.1-10.5 | 2.1 | 10 | 0 | 0 | 0.00 |

| VOL | MMH | AREA | WFLUX | NEAR | NEIGH | ECR | ACT | NO | NO | VELOCITY | TRK | CLS | CNT | G | OVER |
|------|------|------|-------|------|-------|-----|-----|----|----|----------|------|-----|-----|-----|------|
| SCAN | MMH2 | MMH2 | CELL | CLS | ECR | ACT | VOL | CS | FC | EM/S | NH/S | NO | CLS | CTR | C |
| 2 | 1601 | 1.3 | 12.19 | 9.6 | 0.0 | 0.0 | 12 | 4 | 3 | 11.8 | 2.1 | 21 | 2 | 4 | 0 |

Table 4. ACDF Volume Scan Output for Volume Scan No. 3

--- SCAN TIME 122 160827 - 161321 VBL SCAN 3 #2 -145.4 TO 144.3 (DEG)
 TRACK REF TIME 16 742 - 160827 AZM SCAN 8/C EL - 0.4 TO 5.8 (CEL)

NFN = 8, NVMA = 34

FIXED CONTOUR OUTPUT

| CENTROID | | AV | CELL | Z | N | N | SFR | SPR | C | WTR | AREA | VELOCITY | NEAR | MX | MR | SP | | | | |
|----------|-----|-----|------|-----|----|----|-----|-----|---|-----|------|----------|------|------|-----|------|------|----|----|----|
| TRK | AZM | RNG | AZM | RNG | AV | PK | V | S | C | X | L | F | FLUX | ACN | AV | CELL | DIST | HT | ID | IC |
| NO | DEG | KM | DEG | KM | DB | DB | C | C | L | KM | KM | T | MT/H | KM2 | DEC | M/S | KM | KM | NO | NO |
| 2 | 321 | 181 | 322 | 179 | 45 | 51 | 5 | 2 | C | 3.5 | 8.0 | 42 | 6.73 | 0.37 | 257 | 8 | 7.4 | 5 | 0 | 0 |
| 5 | 310 | 203 | 310 | 203 | 36 | 41 | 2 | C | C | 0.0 | 0.0 | C | 0.40 | 0.08 | 999 | 999 | 0.0 | 7 | 0 | 0 |
| 3 | 332 | 216 | 333 | 217 | 37 | 38 | 2 | C | C | 0.0 | 0.0 | C | 0.48 | 0.11 | 274 | 15 | 0.0 | 6 | 0 | 0 |
| 4 | 333 | 162 | 331 | 161 | 42 | 49 | 8 | 3 | 1 | 5.3 | 5.3 | 44 | 4.08 | 0.60 | 258 | 10 | 4.0 | 9 | 4 | 0 |

VOLUME CELL OUTPUT

| CENTROID | | - | - | Z | - | HCT | VBAR | CELL | SPACIAL | (TAN) | CCP | RAC | RAC | CS | ON | C | R | A | | | |
|----------|------|-----|----|----|----|-----|------|------|---------|-------|------|------|-------|-------|-------|------|-----|----|----|---|---|
| TRK | EST | NDR | AV | PK | LW | HI | L | M | EM/S | NM/S | SPRD | A | (SHR) | SFD | VEL | SPD | TR | TR | C | E | |
| NO | KM | KM | DB | DB | DB | DB | W | W | I | CLD | IC | KM | KM2 | (M/K) | PSK | M/S | M/S | NO | NO | P | E |
| 1 | -115 | 144 | 31 | 31 | 31 | 6 | 6 | 6 | 18.1 | 0.6 | 0.00 | 3.5 | 2.4 | 0.0 | -11.1 | 0.0 | 0 | -2 | 4 | 0 | 2 |
| 2 | -119 | 138 | 47 | 51 | 51 | 40 | 4 | 5 | 9 | 11.3 | 2.9 | 0.26 | 10.5 | 1.9 | 0.0 | -7.2 | 2.6 | 0 | 2 | 5 | 4 |
| 3 | -110 | 145 | 44 | 44 | 44 | 4 | 4 | 4 | 4.2 | 1.5 | 0.00 | 3.4 | 2.5 | 0.0 | -1.5 | 3.5 | 0 | 2 | 2 | 0 | |
| 5 | -101 | 149 | 39 | 41 | 41 | 32 | 4 | 5 | 7 | 13.4 | 1.1 | 0.00 | 3.7 | 1.7 | 0.0 | -5.4 | 2.9 | 0 | 2 | 3 | 2 |
| 6 | -83 | 137 | 31 | 31 | 31 | 31 | 3 | 3 | 12.4 | 1.1 | 0.00 | 1.5 | 1.3 | 0.0 | 1.9 | 0.0 | 0 | 1 | 1 | 0 | |
| 7 | -83 | 148 | 38 | 38 | 38 | 36 | 4 | 4 | 14.2 | 5.2 | 0.00 | 12.0 | 1.9 | 0.0 | -4.1 | 5.3 | 0 | 1 | 2 | 1 | |
| 8 | -100 | 188 | 38 | 38 | 38 | 36 | 5 | 5 | 14.5 | 1.8 | 0.00 | 15.2 | 0.0 | 0.0 | -13.6 | 0.0 | 0 | -3 | 0 | 1 | |
| 9 | -73 | 146 | 42 | 44 | 44 | 40 | 4 | 4 | 15.2 | 2.4 | 0.00 | 7.3 | 1.9 | 0.0 | -7.8 | 3.8 | 3 | 1 | 3 | 2 | |
| 14 | -80 | 139 | 37 | 37 | 37 | 37 | 4 | 4 | 11.5 | 3.1 | 0.00 | 4.3 | 1.8 | 0.0 | -6.0 | 1.8 | 0 | -1 | 2 | 0 | |
| 15 | -79 | 134 | 46 | 49 | 49 | 38 | 5 | 6 | 9 | 3.9 | -2.5 | 1.02 | 6.9 | 2.1 | 0.0 | -5.0 | 4.1 | 0 | 1 | 1 | |
| 17 | -86 | 139 | 43 | 46 | 44 | 38 | 4 | 6 | 9 | 4.6 | 1.4 | 1.64 | 6.7 | 1.4 | 0.0 | -9.4 | 4.8 | 0 | 1 | 3 | |
| 20 | -118 | 133 | 42 | 43 | 43 | 42 | 6 | 6 | 8.0 | 2.5 | 0.00 | 5.0 | 1.2 | 0.0 | -0.6 | 3.8 | 0 | -2 | 2 | 0 | |
| 21 | -157 | 130 | 38 | 41 | 41 | 31 | 5 | 7 | 11.8 | 2.1 | 0.00 | 2.3 | 0.0 | 0.0 | -14.4 | 0.5 | 0 | 5 | 0 | | |
| 22 | -113 | 139 | 50 | 50 | 50 | 50 | 4 | 4 | 11.8 | 2.1 | 0.00 | 10.6 | 1.7 | 0.0 | -3.8 | 6.4 | 0 | 2 | 1 | | |
| 23 | -98 | 196 | 37 | 37 | 37 | 37 | 6 | 6 | 11.8 | 2.1 | 0.00 | 4.1 | 0.0 | 0.0 | -14.0 | 0.0 | 0 | 3 | 0 | | |
| 24 | -71 | 144 | 45 | 45 | 45 | 45 | 3 | 3 | 11.8 | 2.1 | 0.00 | 7.6 | 1.8 | 0.0 | -8.9 | 0.6 | 0 | 1 | 1 | | |
| 25 | -151 | 131 | 34 | 36 | 36 | 31 | 5 | 7 | 11.8 | 2.1 | 0.00 | 4.4 | 1.4 | 0.0 | -3.8 | 3.8 | 0 | 5 | 1 | | |
| 27 | -113 | 130 | 37 | 40 | 35 | 34 | 5 | 7 | 11.8 | 2.1 | 0.00 | 14.7 | 1.4 | 0.0 | -5.1 | 6.4 | 0 | 2 | 2 | | |
| 30 | -73 | 131 | 36 | 38 | 38 | 35 | 4 | 6 | 9 | 11.8 | 2.1 | 0.00 | 10.0 | 1.6 | 0.0 | -5.9 | 7.6 | 0 | 1 | 4 | |
| 32 | -76 | 140 | 36 | 38 | 38 | 35 | 6 | 7 | 8 | 11.8 | 0.1 | 0.00 | 6.8 | 1.7 | 0.0 | -5.8 | 5.4 | 0 | 1 | | |
| 33 | -59 | 132 | 32 | 32 | 32 | 32 | 5 | 5 | 11.8 | 2.1 | 0.00 | 7.1 | 2.1 | 0.0 | -4.8 | 0.9 | 0 | 0 | 2 | | |

CLUSTER OUTPUT

| CENTROID | | Z | N | SFR | SPR | DRT | CNT | VELOCITY | SHEAR | MX | MR | SE | CELL | CELL | NO |
|----------|-----|-----|----|-----|-----|-----|-----|----------|--|------|------|------|------|------|------|
| TRK | AZM | RNG | AV | PK | V | X | L | ANG | ID | AV | CELL | MSKM | HT | ID | IC |
| NO | DEG | KM | DB | DB | C | KM | KM | DEC | EM/S <td>NM/S</td> <td>KM</td> <td>NO</td> <td>NO</td> <td>MSKM</td> <td>MSKM</td> | NM/S | KM | NO | NO | MSKM | MSKM |
| 3 | 333 | 164 | 42 | 44 | 1 | 0.0 | 0.0 | C | 1 | 20.2 | 1.6 | 1.9 | 5 | C | C |

| VBL | NMPP | AREA | WFLUX | NEAR | NEIGHBOR | ACT | NO | NO | VELOCITY | TRK | CLS | CNT | 6 | OVER |
|------|------|-------|-------|------|----------|-----|----|----|----------|------|-----|-----|-----|------|
| SCAN | KM2 | KMT/H | CELL | CLST | CCNT | VCL | CS | FC | EM/S | NM/S | NO | CTR | CTR | C |
| 3 | 1607 | 1.3 | 13.52 | 6.0 | 13.7 | 0.0 | 21 | 5 | 4 | 11.0 | 1.8 | 34 | 3 | 5 |

Table 5. ACDT Volume Scan Output for Volume Scan No. 4

SCAN TIME 122 161506 - 162103 VOL SCAN 4 AZ -141.5 TO 110.0 (DEG)
 TRACK REF TIME 1613 3 - 161506 AZM SCAN S/C EL - 0.3 TO 6.6 (DEG)

NFN = 9, NVMX = 44

FIXED CONTOUR OUTPUT

| CENTROID | | AV CELL | | Z | | N N N | | SPR SPR | | C | | WTR AREA | | VELOCITY | | NEAR | | MX PR SP | |
|----------|-----|---------|-----|-----|----|-------|----|---------|---|-----|------|----------|-------|----------|------|------|-----|----------|----|
| TRK | AZM | RNG | AZM | RNG | AV | PK | V | X | L | R | FLX | XSCN | AV | CELL | DIST | HT | ID | ID | |
| NO | DEG | KM | DEG | KM | DB | DB | C | C | L | KM | KM | T | MT/H | KM2 | DEG | M/S | KM | KM | NO |
| 5 | 311 | 199 | 310 | 202 | 39 | 45 | 2 | 1 | 1 | 0.0 | 0.0 | C | 0.97 | 0.14 | 271 | 6 | 0.0 | 7 | 0 |
| 6 | 332 | 212 | 332 | 212 | 34 | 34 | 1 | 0 | 0 | 0.0 | 0.0 | C | 0.06 | 0.02 | 297 | 7 | 0.0 | 5 | 0 |
| 1 | 326 | 170 | 326 | 168 | 44 | 52 | 18 | 3 | 3 | 7.5 | 18.1 | 65 | 11.55 | 1.08 | 250 | 13 | 4.6 | 11 | 2 |
| 3 | 335 | 221 | 335 | 221 | 35 | 35 | 1 | 0 | 0 | 0.0 | 0.0 | C | 0.06 | 0.02 | 237 | 17 | 0.0 | 6 | 0 |

VOLUME CELL OUTPUT

| CENTROID | | Z | | HGT | | VBAR | | CELL | | SPACIAL | | (TAN) | | CCP | | RAC | | CS | | CN | | C | | R | | F | |
|----------|------|-----|----|-----|----|------|---|------|------|---------|------|-------|------|-------|-------|-------|-----|----|----|----|---|---|---|---|---|---|---|
| TRK | EST | NOR | AV | PK | LV | HI | L | M | H | EM/S | NM/S | SPRD | A | (SHR) | SFD | VEL | SPE | TR | TR | E | E | E | E | E | E | E | E |
| NO | KM | KM | DB | DB | DB | DB | W | N | I | OLD | ID | KM | KM2 | (MSK) | MSK | M/S | M/S | NO | NO | P | P | P | P | P | P | P | P |
| 2 | -114 | 139 | 48 | 52 | 52 | 47 | 4 | 5 | 8 | 11.7 | 2.6 | 0.00 | 10.2 | 1.9 | 0.0 | -7.0 | 7.9 | 4 | 1 | 1 | 3 | 2 | | | | | |
| 3 | -104 | 147 | 40 | 40 | 40 | 4 | 4 | 4 | 4 | 5.5 | 3.6 | 0.00 | 9.5 | 4.3 | 0.0 | -3.4 | 0.0 | 0 | 1 | 1 | 0 | 2 | | | | | |
| 5 | -93 | 152 | 32 | 32 | 32 | 6 | 6 | 6 | 17.5 | 5.3 | 0.00 | 9.2 | 0.0 | 0.0 | -14.5 | 0.0 | 0 | 1 | 0 | 1 | 2 | | | | | | |
| 6 | -80 | 140 | 47 | 51 | 51 | 44 | 3 | 4 | 6 | 10.3 | 4.0 | 0.00 | 5.5 | 3.0 | 0.0 | -4.2 | 3.6 | 5 | 1 | 4 | 3 | 2 | | | | | |
| 7 | -76 | 153 | 36 | 36 | 36 | 36 | 4 | 4 | 17.4 | 9.2 | 0.00 | 15.0 | 0.0 | 0.0 | -13.6 | 0.0 | 0 | 1 | 0 | 1 | 2 | | | | | | |
| 8 | -98 | 187 | 34 | 34 | 34 | 34 | 5 | 5 | 5 | 5.7 | -1.3 | 0.00 | 3.8 | 0.0 | 0.0 | -13.9 | 0.0 | 0 | 6 | 0 | 1 | 2 | | | | | |
| 9 | -71 | 149 | 40 | 43 | 43 | 36 | 4 | 4 | 5 | 10.0 | 5.2 | 0.00 | 2.1 | 0.0 | 0.0 | -12.6 | 1.8 | 0 | 1 | 0 | 2 | | | | | | |
| 15 | -75 | 136 | 44 | 48 | 48 | 33 | 5 | 6 | 10 | 8.4 | 1.7 | 0.69 | 7.4 | 1.9 | 0.0 | -5.4 | 5.8 | 5 | 1 | 7 | 5 | 2 | | | | | |
| 17 | -83 | 141 | 40 | 41 | 39 | 41 | 5 | 6 | 7 | 6.3 | 4.3 | 0.00 | 4.2 | 0.0 | 0.0 | -14.1 | 0.2 | 5 | 1 | 0 | 2 | | | | | | |
| 20 | -114 | 135 | 41 | 42 | 42 | 42 | 4 | 4 | 4 | 8.5 | 3.5 | 0.00 | 3.7 | 4.2 | 0.0 | -0.5 | 0.0 | 0 | 1 | 1 | 0 | 2 | | | | | |
| 22 | -109 | 137 | 49 | 49 | 49 | 49 | 4 | 5 | 5 | 11.6 | -2.3 | 0.00 | 8.9 | 2.1 | 0.0 | -4.2 | 6.6 | 4 | 1 | 1 | 2 | | | | | | |
| 23 | -92 | 200 | 35 | 35 | 35 | 35 | 6 | 6 | 13.5 | 6.5 | 0.00 | 5.5 | 0.0 | 0.0 | -14.5 | 0.0 | 0 | 3 | 0 | 1 | 2 | | | | | | |
| 24 | -63 | 144 | 41 | 41 | 41 | 41 | 3 | 3 | 16.1 | 0.3 | 0.00 | 4.0 | 1.9 | 0.0 | -11.6 | 0.0 | 0 | 1 | 1 | 0 | 2 | | | | | | |
| 25 | -149 | 131 | 42 | 45 | 45 | 34 | 5 | 5 | 7 | 8.5 | 0.7 | 0.00 | 9.7 | 1.6 | 0.0 | -8.7 | 3.2 | 6 | 5 | 2 | 2 | | | | | | |
| 27 | -109 | 133 | 47 | 49 | 46 | 49 | 5 | 7 | 10.2 | 5.2 | 0.00 | 2.6 | 2.5 | 0.0 | -4.1 | 3.9 | 7 | 1 | 5 | 2 | 2 | | | | | | |
| 30 | -69 | 135 | 39 | 39 | 39 | 39 | 4 | 4 | 11.5 | 6.5 | 0.00 | 4.1 | 2.0 | 0.0 | -5.9 | 1.2 | 0 | 1 | 2 | 0 | 2 | | | | | | |
| 32 | -70 | 142 | 39 | 39 | 39 | 39 | 3 | 3 | 13.7 | 3.0 | 0.00 | 2.7 | 2.5 | 0.0 | -6.3 | 2.5 | 0 | 1 | 2 | 0 | 2 | | | | | | |
| 33 | -57 | 132 | 33 | 33 | 33 | 33 | 6 | 6 | 6 | 6.7 | 2.2 | 0.00 | 2.7 | 3.8 | 0.0 | -7.4 | 0.0 | 0 | 0 | 1 | 0 | 2 | | | | | |
| 34 | -161 | 127 | 33 | 34 | 24 | 33 | 5 | 6 | 7 | 11.0 | 1.8 | 0.00 | 8.9 | 0.0 | 0.0 | -7.1 | 7.1 | 0 | 5 | 0 | 2 | 1 | | | | | |
| 35 | -113 | 129 | 39 | 39 | 39 | 39 | 4 | 4 | 11.0 | 1.8 | 0.00 | 3.6 | 0.0 | 0.0 | -15.3 | 0.0 | 0 | 1 | 0 | 1 | 1 | | | | | | |
| 36 | -101 | 147 | 47 | 47 | 47 | 47 | 4 | 4 | 11.0 | 1.8 | 0.00 | 3.4 | 2.7 | 0.0 | -6.9 | 0.0 | 0 | 1 | 0 | 1 | 1 | | | | | | |
| 37 | -97 | 141 | 34 | 34 | 34 | 34 | 4 | 4 | 11.0 | 1.8 | 0.00 | 6.5 | 2.5 | 0.0 | -6.5 | 2.3 | 0 | 1 | 3 | 0 | 1 | | | | | | |
| 38 | -157 | 123 | 32 | 32 | 22 | 32 | 7 | 7 | 11.0 | 1.8 | 0.00 | 6.3 | 0.0 | 0.0 | -14.4 | 0.0 | 0 | 0 | 0 | 1 | 1 | | | | | | |
| 40 | -108 | 132 | 46 | 50 | 50 | 36 | 5 | 6 | 10 | 11.0 | 1.8 | 0.09 | 9.4 | 1.9 | 0.0 | -6.3 | 4.6 | 7 | 1 | 2 | 4 | 1 | | | | | |
| 42 | -114 | 137 | 42 | 45 | 45 | 33 | 7 | 8 | 11.0 | 1.8 | 0.00 | 9.9 | 0.0 | 0.0 | -9.2 | 6.6 | 4 | 1 | 0 | 3 | 1 | | | | | | |
| 44 | -65 | 132 | 36 | 39 | 39 | 32 | 7 | 7 | 8 | 11.0 | 1.8 | 0.00 | 6.4 | 2.1 | 0.0 | -4.6 | 5.4 | 0 | 1 | 4 | 2 | 1 | | | | | |

CLUSTER OUTPUT

| CENTROID | | Z | | N SPR | | SPR | | ORT | | CNT | | VELOCITY | | SPEAR | | MX | | PR | | SP | | CELL | | CELL | | NO | |
|----------|-----|-----|----|-------|---|-----|-----|-----|----|------|------|----------|----|-------|------|-------|------|----|--|----|--|------|--|------|--|----|--|
| TRK | AZM | RNG | AV | PK | V | X | L | ANG | ID | AV | CELL | MSKM | HT | ID | ID | ROT. | DIV. | RD | | | | | | | | | |
| NO | DEG | KM | DB | DB | C | KM | KM | DEG | | EM/S | NM/S | KM | NE | NO | MSKM | MSKM | ES | | | | | | | | | | |
| 4 | 321 | 178 | 47 | 52 | 3 | 0.9 | 2.5 | 291 | 1 | 11.7 | -1.4 | 1.8 | 11 | C | C | 0.00 | 0.00 | 2 | | | | | | | | | |
| 5 | 330 | 161 | 45 | 51 | 3 | 0.2 | 4.1 | 304 | 1 | 9.2 | 5.5 | 2.3 | 10 | C | C | -0.47 | 4.79 | 3 | | | | | | | | | |
| 6 | 311 | 199 | 42 | 45 | 1 | 0.0 | 0.0 | C | 5 | 6.3 | -0.1 | 1.6 | 7 | C | C | 0.00 | 0.00 | C | | | | | | | | | |
| 7 | 321 | 172 | 47 | 50 | 2 | 0.0 | 0.0 | C | 1 | 9.0 | 7.2 | 2.3 | 10 | C | C | 0.00 | 0.00 | C | | | | | | | | | |

VOL HMMF AREA WFLUX NEAR NEIGHBOR ACT NO NO VELOCITY TRK CLS CNT C OVER
 SCAN KKM2 KMT/H CELL CLST CONT VCL CS FC EM/S NM/S NO CTR CTR C
 -4 1613 1.5 15.71 5.0 0.0 0.0 26 4 -2 11.3 3.0 44 7 0 0 0 0 0 0

Table 6. ACDT-WEATRK From 1 Comparison for Case Study No. 1

| Algorithm | Contour Region No. or Start Cell No. | Azimuth | Range (km) | Max Height (km) | Centroid Direction | Speed (M/S) | Max. up- Reflectivity | Average Reflectivity |
|------------------|--|---------|---------------|--------------------|-----------------------|-------------|--------------------------|-------------------------|
| <u>Time 1555</u> | | | | | | | | |
| ACDT | 1 | 330 | 167 | 12 | - | - | 47 | 50 |
| WEATRK | 1 | 330 | 160 | 10.4 | - | - | 51 | |
| ACDT | 2 | 319 | 188 | 10 | - | - | 46 | |
| WEATRK | 2 | 318 | 186 | 9.6 | - | - | 46 | 46 |
| WEATRK | 3 | 324 | 184 | 9.5 | - | - | 46 | |
| ACDT | 3 | 329 | 217 | 6 | - | - | 44 | 48 |
| WEATRK | 4 | 330 | 214 | 4.6 | - | - | 48 | |
| <u>Time 1601</u> | | | | | | | | |
| ACDT | 4 | 237 | 163 | 10 | 314 | 12 | 49 | |
| ACDT | 1 | 332 | 165 | 3 | 296 | 12 | 55 | 57 |
| WEATRK | 1 | 331 | 156 | 10.4 | 243 | 10 | 52 | |
| ACDT | 2 | 320 | 185 | 9 | 258 | 15 | 47 | |
| WEATRK | 2 | 320 | 180 | 10.2 | 284 | 22 | 53 | |
| ACDT | 3 | 331 | 217 | 4.9 | 238 | 17 | 44 | |
| WEATRK | 4 | 332 | 214 | 4 | 236 | 20 | 53 | |
| <u>Time 1608</u> | | | | | | | | |
| ACDT | 1 | 333 | 162 | 9 | 258 | 10 | 49 | 56 |
| WEATRK | 1 | 331 | 154 | 10.0 | 288 | 9 | 51 | |
| ACDT | 2 | 321 | 181 | 9 | 257 | 8 | 51 | |
| WEATRK | 2 | 321 | 176 | 9.8 | 279 | 14 | 54 | |
| ACDT | 3 | 332 | 216 | 6 | 274 | 15 | 36 | 49 |
| WEATRK | 4 | 333 | 212 | 4.9 | 243 | 16 | 40 | |
| ACDT | 5 | 310 | 203 | 7 | - | - | 41 | 43 |
| WEATRK | 5 | 311 | 200 | 4.4 | - | - | 42 | |

Table 6. ACDT-WEATRK Product Comparison for Case Study No. 1 (Contd)

| Algorithm | Contour Region No. or Storm Cell No. | Azimuth ° | Range (km) | Max Height (km) | Centroid Direction | Speed (M/S) | Maximum Reflectivity | Verified Reflectivity |
|-----------|--|--------------|---------------|--------------------|-----------------------|-------------|-------------------------|--------------------------|
| ACDT | 1 | 326 | 170 | 11 | 250 | 13 | 52 | |
| WEATRK | 2 | 322 | 170 | 11.1 | 286 | 16 | 55 | 55 |
| WEATRK | 1 | 334 | 152 | 9.8 | 277 | 10 | 54 | |
| ACDT | 5 | 311 | 199 | 7 | 271 | 6 | 45 | |
| WEATRK | 5 | 309 | 202 | 7.2 | 44 | 12 | 42 | 46 |
| WEATRK | 6 | 313 | 194 | 3.9 | - | - | 46 | |
| ACDT | 3 | 335 | 221 | 6 | 327 | 17 | 35 | |
| ACDT | 6 | 332 | 212 | 7 | 297 | 7 | 34 | |

Before the data are compared, it is necessary to discuss the differences in the algorithms' processing schemes. Since WEATRK tracks three-dimensional storm cells, that are large relative to the volume cells tracked by ACDT, the centroid position of the storm cell will be different from that of the contour region given by ACDT.

The centroid locations of the various ACDT contour regions, and WEATRK storm cells are plotted in Figures 1, 2, 3, and 4. Although the centroid locations of the WEATRK storm cells and the ACDT contour regions are derived differently they both represent three-dimensional reflectivity-weighted entities, and are hard to locate on two-dimensional single elevation angle plots. In viewing these figures it must be noted that the contoured data field is slightly smoothed by the coordinate conversion and plotting routines.

Table 6 reveals that the maximum reflectivity values reported by WEATRK are slightly higher than those from ACDT. This is due to the two range gate averaging performed by the ACDT.

The maximum echo heights reported by the ACDT are generally close to those reported by WEATRK. There are, however, some differences of more than 1.5 km (that is, contour region No. 1 at 1555, contour region No. 5 at 1608). These might be explained by the ACDT finding a 3-dB peak in the next higher elevation azimuth scan that does not exceed the WEATRK criterion of reflectivity above threshold in 14 contiguous range gates.

The velocity difference between the ACDT contour region centroids and the WEATRK storm cell centroids shows a bias of +11.8° and -1.7 m/sec. These are acceptable since the centroid positioning error for this data is ± 1.5 km.

The net effect of these differences is negligible as both the contour regions and the storm cells propagate in approximately the same direction. Figure 5 is the contour plot for the first volume scan of this case study, with the centroid locations of the ACDT contour regions and WEATRK storm cells for all four volume scans labeled. It is interesting to note the apparent reversal in the motion of contour region 1 at 1615. This is obviously due to the merging of contour regions 1 and 2.

4.1.2 SPATIAL CORRELATIONS

Further analysis of the ACDT output reveals that an average 52% of all volume cells are detected at only one height. Out of the nine volume cells tracked over all four volume scans, only volume cell 2 was detected at more than one height at all times.

Some of these "single height" volume cells appear to be oriented in such a way as to suggest that they might be vertically correlated with neighboring "single height" cells (for example, cells 9 and 15 at 1601, 6 and 17 at 1608). This might imply we have reason to doubt the validity of the vertical correlation function used in the

algorithm. The following comments from Gustafson and Crane, ⁷ page 7, concur with this reasoning: "Relaxation of the height separation criteria of the association logic to accommodate large elevation steps could cause invalid associations such as that of an immature cell at a mid-level with the cirrus overhang from a nearby mature storm. Clearly a trade-off is required; thus, the weight of the height component of the association function is defined such that a separation of between 2.5 and 3.0 km will make an association difficult (that is, require close agreement between the other components), and a separation greater than 3 km will cause the association to be rejected."

CONTOURS OF DBZ

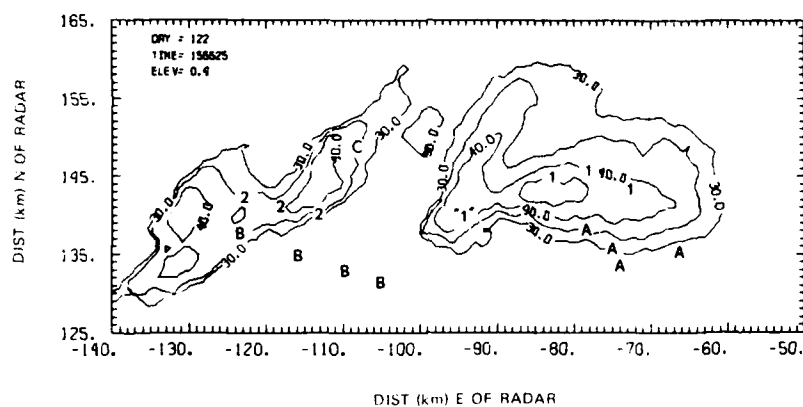


Figure 5. ACDDT Contour Region (numbered) and WEATRK Storm Cell (lettered) Centroid Locations for Volume Scans 1-4. Motion is from left to right, location marked "1" is centroid location of merged contour regions 1 & 2 in Volume Scan No. 4

The data were collected at 0.7° elevation angle steps; thus by using the 4:3 earth beam refraction correction we find the height difference between elevation angles is 2.5 km at a range of 150 km and 4.0 km at 230 km.

Another factor that may be contributing to the vertical correlation problem is that the height computations for some features appear to be wrong. Although most of the heights are correct within the resolution of the algorithm (1 km), there are a few cases where the height given for a volume cell is in error even when truncated to the nearest kilometer. Table 7 illustrates this discrepancy.

In studying the cluster output for this case it is apparent that 83% of the clusters are not correlated in time, and no single cluster is tracked throughout the entire 4 volume scans.

Table 7. Comparison of Height Estimates of Selected Volume Cells From ACDT and 4/3 Earth Correction for the Lowest Two Elevation Angles (α)

| Cell No. | Volume Scan No. | Range | ACDT Height | 4/3 Earth $\alpha = 0.4^\circ$ | 4/3 Earth $\alpha = 1.3^\circ$ |
|----------|-----------------|-------|-------------|--------------------------------|--------------------------------|
| 1 | 1 | 194 | 5 | 3.9 | 6.9 |
| 9 | 1 | 167 | 4 | 3.1 | 5.6 |
| 9 | 2 | 167 | 2 | 3.1 | 5.6 |

Figure 6 is a plot of the positions and trajectories of the volume cells in contour No. 1 starting with volume scan No. 1. These volume cell tracks all look plausible, although it is interesting to note the movement of volume cell 16 around 17 and the almost complete reversal of direction of cell 15.

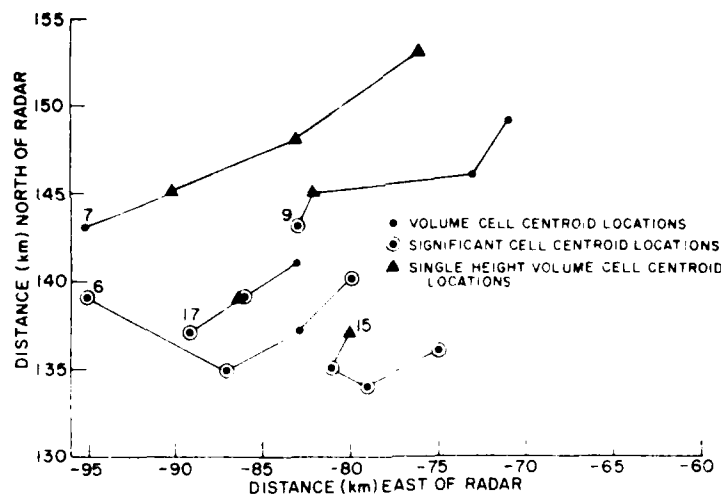


Figure 6. ACDT Volume Cell Centroid Trajectories for Contour Region No. 1. For volume scans 1-4

Figure 7 is a plot of the vertical extent of selected volume cells throughout the period of interest. This diagram illustrates the rapid structural changes in several volume cells. Cells 6 and 17 seem to alternately lose and gain their significance in volume scans 2 through 4. Cells 7 and 9 behave erratically between volume scans 1 and 2, going from a multi-height entity to a single height entity at

a lower elevation. Volume cell No. 5 is an example of a short lived significant cell, one which does not decay the way one might expect, that is, with reflectivity gradually lowering in time. The behavior of volume cell 20 on the other hand might be indicative of a decaying cell. Volume cell numbers 1, 3, 8 are examples of single height cells that are tracked over several volume scans. Volume cell No. 2 is an example of a relatively long lived significant cell. Volume cell 15 could be an example of a growing storm cell.

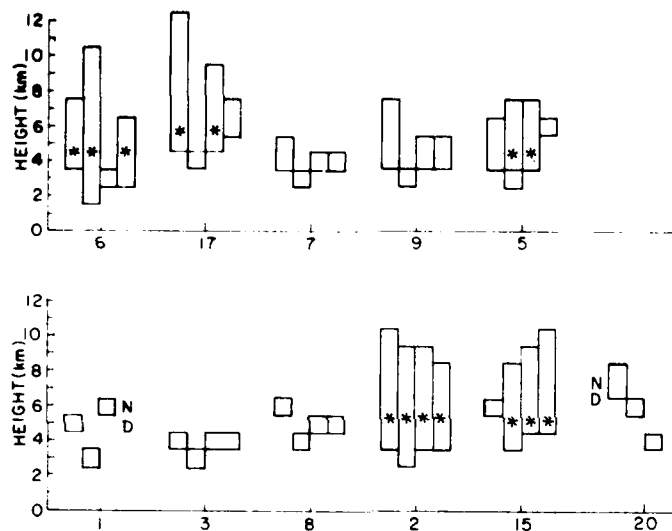


Figure 7. Volume Cell Vertical Extent for Volume Scans 1-4.
(* signifies significant cells, ND - Volume Cell not defined)

4.1.3 TEMPORAL CORRELATIONS

One check of the reliability of a tracking algorithm is the examination of the ratio of the nearest neighbor distance between cells and the distance each cell travels between observation times. This ratio should be greater than 1 to have any meaningful significance. Another parameter to consider is the ratio of the nearest neighbor distance and the average cell diameter to give another indication of possible cell overlap. These ratios were computed for all the nearest neighbor volume cells within a contour region.

Table 3 contains a listing of these ratios for all the nearest neighbor cells that had a lifetime of more than two volume scans (~ 12 min).

Table 8. Compilation of Volume Cell Overlap Ratios,
for Nearest Neighbor Cells

| Time | Contour | Cell Group | d/st | $d/2r$ |
|------|---------|------------|---------------------------------|---------------------------------|
| 1601 | 2 | 1-2 | 1.5 | 2.2 |
| | 2 | *2-20 | 1.2 | 1.5 |
| | 2 | *3-5 | 1.2 | 1.2 |
| | 1 | *7-9 | 2.1 | 2.2 |
| | 4 | *6-15 | 1.7 | 1.7 |
| 1608 | 1 | *7-9 | 0.3 | 0.4 |
| | 1 | *6-17 | 1.1 | 1.9 |
| | 1 | 6-15 | 2.2 | 2.4 |
| | 2 | *3-5 | 2.0 | 2.5 |
| | 2 | *1-20 | 2.1 | 3.7 |
| 1615 | 1 | *2-20 | 2.2 | 1.3 |
| | 1 | *6-17 | 0.9 | 1.3 |
| | 1 | *30-32 | 1.4 | 0.1 |
| | 1 | 15-32 | 1.9 | 3.1 |
| | 1 | 24-30 | 2.0 | 4.8 |
| | 1 | *22-27 | 0.9 | 1.4 |
| | 1 | *9-32 | 1.6 | 4.1 |
| | 1 | *7-9 | 1.1 | 1.9 |
| | 1 | 3-22 | 2.8 | 3.2 |
| | | | $\overline{\frac{d}{st}} = 1.4$ | $\overline{\frac{d}{2r}} = 1.9$ |

* Cell groups are counted twice in overall average (that is, is, cell No. 2 is the nearest neighbor to cell No. 20 and vice versa)

The following variables are used to compute these ratios:

- d = Nearest neighbor separation distance (km),
- \bar{s} = Average cell speed over the volume scan (km/s),
- t = Volume scan time (s),
- r = Average cell radius (km).

The overall average for the nearest neighbor distance over the distance each cell travels between observation times ($\frac{d}{st}$) is 1.4, the overall average for the ratio of nearest neighbor distance to cell diameter ($\frac{d}{2r}$) is 1.9. The error in determining cell position due to the radar beam width is ± 1.5 km at a range of 175 km. This positioning error results in an uncertainty of ± 3.0 in $\frac{d}{st}$ and ± 1.8 $\frac{d}{2r}$. Considering these uncertainties, it is obvious that the above ratios are not large enough to demonstrate that the algorithm can distinguish between adjacent volume cells in subsequent volume scans.

4.2 Case Study No. 2

The second case study consists of four volume scans, recorded from 1534-1557 CST on 10 April 1979. The thunderstorm observed at this time extended in a complex band from the northeast to southwest of the radar. Figure 8 is a contour plot of a small section of this band. The closest identifiable 30-dBz contour was at a range of 20 km.

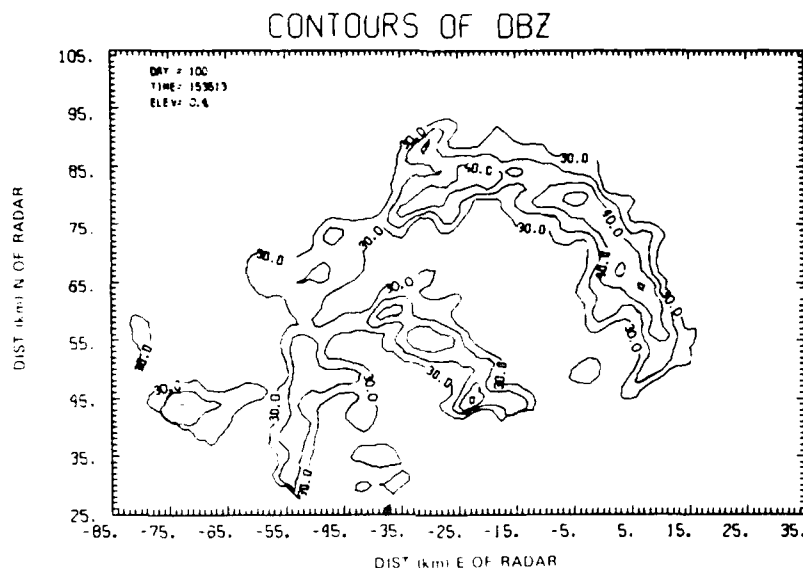


Figure 8. Reflectivity Contour Plot for Volume Scan Beginning at 1534

A synopsis of the ACDT output (Appendix A) can be seen in Table 9. The high number of contours and volume cells in Table 6 confirms the complex nature of the storm system on this day. The number of fixed contour regions for the time period of interest never drops below 33, yet only three of these are correlated throughout all four volume scans. On the average 77% of all contour regions are not temporally correlated.

The number of volume cells detected for each volume scan is also very large. It was found that on average 49% of all volume cells were uncorrelated in time and 55% were uncorrelated vertically (that is, detected at only one height). There were 21 volume cells that were followed for the entire time, yet only four of these (numbers 42, 53, 126, 131) had vertical continuity at all times. Considering this it is not surprising that 56% of the clusters in this case showed no temporal continuity. This case was run again with 35 dBz as a threshold; the effect of which was

to reduce the number of contour regions from 39 to 32 without changing significantly the number of volume cells that were uncorrelated in time. In comparison, when the WEATRK algorithm was run with a 35-dBz threshold over the same data, it detected 12 storm cells, and tracked 8 of these throughout this time period. It must be noted, that WEATRK only lists the attributes for what it determines to be the 12 most significant storm cells.

In addition, ACDT appears to have difficulties in identifying and tracking significant cells in this case. There are 40 significant cells identified over the period of interest, yet only one of these (number 126) is detected in all four volume scans. Over all, 88% of the significant cells are not correlated in time.

Table 9. Synopsis of the ACDT Algorithm Output for 1534-1557 (CST) on 10 April 1979

| Volume Scan No. | No. of Contour Regions | | No. of Volume Cells | | No. of Clusters | |
|-----------------|------------------------|-----|---------------------|-----|-----------------|-----|
| | Total | New | Total | New | Total | New |
| 1 | 39 | - | 148 | - | 24 | - |
| 2 | 37 | 27 | 148 | 77 | 19 | 8 |
| 3 | 34 | 24 | 113 | 51 | 18 | 11 |
| 4 | 33 | 29 | 140 | 72 | 23 | 15 |

5. SUMMARY AND CONCLUSIONS

The ACDT behaves as designed, that is, it locates 3 dB peaks, defines contours, groups clusters, and tracks these entities. Although not all of the individual 3 dB peaks can be identified in the contour plots presented in this report, they can be located in the higher resolution raw data.

It is apparent that the algorithm is experiencing several problems when applied to our data sets; it has however, proved to yield good results using 3 to 5 min volume scan repeat time with greater vertical resolution (Crane and Hardy,¹⁰ Crane¹¹). It is thought that several of the problems in this analysis such as, uncorrelated volume cells, single height cells, and uncorrelated significant cells are due to inadequate temporal (6-min volume scan repeat time) and/or inadequate vertical resolution (as much as 2.8 km at ranges of 230 km).

11. Crane, R. K. (1976) Radar Detection of Thunderstorm Hazards for Air Traffic Control, Vol. I Storm Detection, Project Report ATC-67, Vol. I, MIT Lincoln Laboratory, Lexington, Massachusetts, FAA-RD-76-52; AD A032732.

Previous studies have only been concerned with data out to 150 km (Crane and Hardy¹⁰). Gustafson¹² concurs with these speculations regarding possible areas of algorithm breakdown.

An average 50% of the volume cells detected by the ACDT are not correlated with another volume cell in the next volume scan. Yet, at the same time the ACDT tracked some single height volume cells over the entire four volume scans of case study No. 1 (that is, cells 3 and 8).

The association of volume cells of considerable vertical extent (that is, > 4 km) in one volume scan to those of little vertical extent (that is, < 1 km) in the next volume scan (that is, 6, 17, 9, 5 in Figure 7) causes us to question the ability of the algorithm to vertically correlate the 3-dB peaks and to adequately track these volume cells.

The ratio of the nearest neighbor distance to the distance an average volume cell travels between observation times is shown to be small when compared to the relative error in determining the volume cell positions. This might explain the difficulties that the ACDT had with cell tracking.

The fact that ACDT sometimes detected higher storm cell peaks is not thought to be a significant advantage over WEATRK as these higher peaks are small (less than 14 range gates) in horizontal extent.

Crane³ found the average lifetime for a significant cell to be approximately 30 minutes. We found the average significant cell to have a lifetime close to 10 minutes.

Crane and Hardy¹⁰ state that the volume cell clusters may be the most important feature for analyzing storm structure. In our analysis 69% of the clusters were uncorrelated in time, suggesting that they may not be quite as important here. This is obviously a product of the difficulties the ACDT has with the elements within the clusters, namely the volume cells.

Finally, a few comments on the software itself. It was found that the subroutines for the ACDT contain a substantial amount of residual developmental code. The subroutines are not modular, hence it is difficult to make changes to the processing scheme without altering the code in several subroutines. The algorithm currently runs at approximately two times real time for the simple case and three times real time for the more complex case. However, if this algorithm were to be used operationally, an entirely new software package would be needed; preferably a modular one designed for speed and efficiency.

12. Gustafson, G. B. (1982) Personal communication.

It is apparent that more work must be done to determine what radar data processing methods would yield the best results for a given meteorological scale. WEATRK tracks the large scale features of a storm complex, while ACDT tracks much smaller entities to presumably yield a description of the internal structure of a storm complex. The ACDT was initially developed to process up to 512 volume cells at one time. It is obvious that processing this amount of data is not possible in a real-time environment. To rectify this problem, Crane³ recommends that the subroutines for cell detection and tracking be maintained while the number of cells be reduced by increasing the reflectivity threshold and by incorporating the tangential shear information in the decision process for saving the most important 12 to 16 cells. It would be more consistent with algorithm development to specify a larger peak size, since raising the threshold level would tend to eliminate growing volume cells.

Since it may well be useful to identify elements within storms, such as significant cells, one might consider an algorithm with resolution capabilities between the two algorithms discussed herein. Perhaps if ACDT were modified to track 6 to 10 dBz peaks, or WEATRK were modified to operate with several thresholds, storm structure would be more readily apparent. If the reflectivity peak processing method were to be explored further it would be prudent to write an algorithm in which the peak size would be an input variable. This would enable the researcher to specify a peak size (feature size) that was consistent with the spatial and temporal resolution of the data set. This type of algorithm could be run repeatedly over the same data altering the peak size to first, observe the large scale features of the storm, then to detect and track the feature of interest, and lastly to determine when the algorithm breaks down (that is, no longer can correlate its derived features).

In reviewing our case studies one can see that it might be necessary to either fine tune the ACDT contour region threshold for each case study, or specify a permissible reflectivity range around the threshold. This would eliminate extraneous contour regions, and eliminate insignificant merges and splits of contour regions due to small fluctuations of the reflectivity field.

The Automatic Cell Detection and Tracking algorithm (ACDT) developed by Crane^{1,2,3,4} has been evaluated by carefully examining two case studies taken from the 1979 JDOP program. The output products from the ACDT were compared to raw data and to the products from the AFGL storm tracking algorithm WEATRK. We found that the ACDT performs unsatisfactorily when constrained to a 5 to 6 min volume scan repeat time, and when it is required to perform out to a range of 230 km. Therefore, we do not recommend its inclusion in the NEXRAD system at this time.

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12. Gustafson, G. B. (1982) Personal communication.

Appendix A

ACDT Algorithm Output

Table A1. ACDT Volume Scan Output for Volume Scan No. 1, Case Study No. 2

| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|--------------------------------|-----|-----|-----|-----|----|----|----|---|------|--------------------------------------|------|-----|------|------|-----|-----|------|------|----|---------------------------------|----|--|--|--|--|--|--|--|--|
| SCAN TIME 100 153447 - 154005 | | | | | | | | | | VOL SCAN 1 47 - 39.3 TO 31.9 (DEG) | | | | | | | | | | | | | | | | | | | |
| TRACK REF TIME 153447 - 153447 | | | | | | | | | | AZM SCAN 11/0 EL * 0.4 TO 11.8 (DEG) | | | | | | | | | | | | | | | | | | | |
| FIXED CONTROL OUTPUT | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| CENTROID AV CELL 2 | | | | | | | | | | N A A S P A C P R C | | | | | | | | | | ATE AREA VELOCITY NEAR MX ME SF | | | | | | | | | |
| TRK | AZM | RAO | AZM | RAO | AV | FX | V | S | C | X | L | R | FLX | X | Y | AV | CELL | DIST | HT | ID | ID | | | | | | | | |
| NO | DEG | KM | DEG | KM | DE | DE | C | C | L | KM | KM | I | MT/E | KM2 | DEG | M/S | KM | KM | AC | AC | | | | | | | | | |
| 1 | 60 | 146 | 59 | 147 | 30 | 34 | 0 | 0 | 0 | 0.0 | 0.0 | 0 | 0.27 | 0.10 | 559 | 999 | 0.0 | 2 | 0 | 0 | | | | | | | | | |
| 2 | 67 | 19 | 68 | 28 | 30 | 32 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.02 | 0.01 | 559 | 999 | 0.0 | 0 | 0 | 0 | | | | | | | | | |
| 3 | 292 | 54 | 292 | 65 | 37 | 40 | 2 | 1 | 1 | 4.5 | 4.4 | 34 | 2.05 | 0.49 | 559 | 999 | 5.2 | 2 | 0 | 0 | | | | | | | | | |
| 4 | 44 | 126 | 44 | 127 | 34 | 34 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.28 | 0.09 | 559 | 999 | 0.0 | 1 | 0 | 0 | | | | | | | | | |
| 5 | 51 | 97 | 51 | 100 | 35 | 35 | 3 | 1 | 1 | 0.2 | 4.5 | 61 | 0.15 | 0.04 | 559 | 999 | 0.0 | 2 | 0 | 0 | | | | | | | | | |
| 6 | 60 | 53 | 61 | 90 | 37 | 32 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.12 | 0.03 | 559 | 999 | 0.0 | 1 | 0 | 0 | | | | | | | | | |
| 7 | 244 | 237 | 243 | 267 | 37 | 37 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.17 | 0.04 | 559 | 999 | 0.0 | 4 | 0 | 0 | | | | | | | | | |
| 8 | 62 | 122 | 62 | 123 | 32 | 32 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.15 | 0.05 | 559 | 999 | 0.0 | 1 | 0 | 0 | | | | | | | | | |
| 9 | 40 | 152 | 42 | 182 | 31 | 31 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.04 | 0.02 | 559 | 999 | 0.0 | 3 | 0 | 0 | | | | | | | | | |
| 10 | 55 | 121 | 55 | 121 | 30 | 43 | 2 | 1 | 1 | 8.7 | 3.7 | 16 | 0.24 | 0.32 | 559 | 999 | 7.6 | 5 | 0 | 0 | | | | | | | | | |
| 11 | 69 | 129 | 69 | 129 | 33 | 32 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.03 | 0.01 | 559 | 999 | 0.0 | 1 | 0 | 0 | | | | | | | | | |
| 12 | 71 | 200 | 71 | 200 | 31 | 31 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.05 | 0.02 | 559 | 999 | 0.0 | 4 | 0 | 0 | | | | | | | | | |
| 13 | 72 | 214 | 72 | 214 | 31 | 31 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.07 | 0.01 | 559 | 999 | 0.0 | 4 | 0 | 0 | | | | | | | | | |
| 14 | 147 | 14 | 153 | 15 | 14 | 34 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.14 | 0.03 | 559 | 999 | 0.0 | 0 | 0 | 0 | | | | | | | | | |
| 15 | 233 | 266 | 234 | 267 | 41 | 44 | 4 | 2 | 2 | 2.8 | 7.5 | 65 | 2.22 | 0.53 | 559 | 999 | 0.0 | 7 | 0 | 0 | | | | | | | | | |
| 16 | 236 | 139 | 235 | 194 | 35 | 44 | 4 | 2 | 2 | 2.8 | 7.5 | 65 | 2.22 | 0.53 | 559 | 999 | 0.0 | 6 | 0 | 0 | | | | | | | | | |
| 17 | 249 | 201 | 249 | 201 | 30 | 33 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.17 | 0.06 | 559 | 999 | 0.0 | 4 | 0 | 0 | | | | | | | | | |
| 18 | 245 | 48 | 245 | 48 | 33 | 32 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.01 | 0.00 | 559 | 999 | 0.0 | 0 | 0 | 0 | | | | | | | | | |
| 19 | 304 | 60 | 302 | 61 | 40 | 51 | 25 | 5 | 7 | 7.9 | 4.5 | 42 | 3.00 | 0.54 | 559 | 999 | 4.5 | 7 | 0 | 0 | | | | | | | | | |
| 20 | 252 | 153 | 253 | 152 | 31 | 31 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.08 | 0.03 | 559 | 999 | 0.0 | 2 | 0 | 0 | | | | | | | | | |
| 21 | 256 | 124 | 257 | 123 | 34 | 37 | 0 | 1 | 1 | 0.0 | 0.0 | 0 | 0.31 | 0.10 | 559 | 999 | 0.0 | 3 | 0 | 0 | | | | | | | | | |
| 22 | 252 | 143 | 243 | 122 | 32 | 32 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.41 | 0.11 | 559 | 999 | 0.0 | 2 | 0 | 0 | | | | | | | | | |
| 23 | 269 | 108 | 268 | 105 | 36 | 41 | 0 | 1 | 0 | 1.4 | 10.5 | 15 | 1.30 | 0.33 | 559 | 999 | 0.0 | 6 | 0 | 0 | | | | | | | | | |
| 24 | 292 | 75 | 291 | 74 | 32 | 32 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.01 | 0.00 | 559 | 999 | 0.0 | 0 | 0 | 0 | | | | | | | | | |
| 25 | 309 | 24 | 316 | 25 | 36 | 40 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.10 | 0.02 | 559 | 999 | 0.0 | 1 | 0 | 0 | | | | | | | | | |
| 26 | 314 | 37 | 322 | 37 | 39 | 47 | 13 | 3 | 3 | 3.6 | 7.0 | 117 | 0.55 | 0.16 | 559 | 999 | 7.6 | 8 | 0 | 0 | | | | | | | | | |
| 27 | 306 | 53 | 306 | 51 | 32 | 32 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.01 | 0.00 | 559 | 999 | 0.0 | 0 | 0 | 0 | | | | | | | | | |
| 28 | 305 | 28 | 305 | 25 | 31 | 21 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.04 | 0.01 | 559 | 999 | 0.0 | 1 | 0 | 0 | | | | | | | | | |
| 29 | 316 | 61 | 312 | 53 | 35 | 35 | 0 | 1 | 1 | 0.0 | 0.0 | 0 | 0.07 | 0.02 | 559 | 999 | 0.0 | 5 | 0 | 0 | | | | | | | | | |
| 30 | 312 | 54 | 311 | 54 | 32 | 34 | 2 | 1 | 1 | 0.0 | 0.0 | 0 | 0.06 | 0.02 | 559 | 999 | 0.0 | 1 | 0 | 0 | | | | | | | | | |
| 31 | 319 | 91 | 319 | 91 | 34 | 34 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.08 | 0.02 | 559 | 999 | 0.0 | 1 | 0 | 0 | | | | | | | | | |
| 32 | 357 | 51 | 357 | 50 | 34 | 35 | 0 | 1 | 1 | 0.0 | 0.0 | 0 | 0.04 | 0.02 | 559 | 999 | 0.0 | 0 | 0 | 0 | | | | | | | | | |
| 33 | 0 | 51 | 359 | 54 | 32 | 32 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.00 | 0.00 | 559 | 999 | 0.0 | 3 | 0 | 0 | | | | | | | | | |
| 34 | 347 | 83 | 341 | 78 | 39 | 47 | 15 | 1 | 11.6 | 9.13 | 2 | 53 | 4.27 | 0.69 | 559 | 999 | 6.5 | 6 | 0 | 0 | | | | | | | | | |
| 35 | 17 | 59 | 18 | 58 | 31 | 31 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.01 | 0.00 | 559 | 999 | 0.0 | 0 | 0 | 0 | | | | | | | | | |
| 36 | 11 | 43 | 13 | 44 | 44 | 45 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.15 | 0.03 | 559 | 999 | 0.0 | 0 | 0 | 0 | | | | | | | | | |
| 37 | 20 | 45 | 20 | 44 | 33 | 33 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.01 | 0.00 | 559 | 999 | 0.0 | 0 | 0 | 0 | | | | | | | | | |
| 38 | 5 | 67 | 8 | 68 | 60 | 45 | 16 | 3 | 7 | 5.6 | 8.4 | 120 | 2.68 | 0.29 | 559 | 999 | 4.7 | 7 | 0 | 0 | | | | | | | | | |
| 39 | 26 | 96 | 26 | 95 | 38 | 38 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.13 | 0.04 | 559 | 999 | 0.0 | 1 | 0 | 0 | | | | | | | | | |

Table A1. ACDT Volume Scan Output for Volume Scan No. 1, Case Study No. 2
(Cont'd)

| VOLUME SCAN OUTPUT | | | | | | | | | | | | | | | | | | | |
|--------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| TRK | ACM | PAG | AV | PK | LR | HI | LN | H | W | W | W | W | W | W | W | W | W | W | W |
| NO. | NO. | NO. | NO. | NO. | NO. | NO. | NO. | NO. | NO. | NO. | NO. | NO. | NO. | NO. | NO. | NO. | NO. | NO. | NO. |
| 1 | 41 | 92 | 37 | 37 | 37 | 37 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 2 | 42 | 132 | 31 | 31 | 31 | 31 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| 3 | 43 | 123 | 32 | 32 | 32 | 32 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 4 | 44 | 127 | 34 | 34 | 34 | 34 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 5 | 47 | 131 | 34 | 34 | 34 | 34 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| 6 | 48 | 22 | 32 | 32 | 32 | 32 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| 7 | 50 | 95 | 33 | 33 | 33 | 33 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 8 | 51 | 113 | 34 | 34 | 34 | 34 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 9 | 52 | 122 | 40 | 42 | 42 | 34 | 1 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| 10 | 56 | 122 | 38 | 38 | 38 | 38 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 11 | 56 | 123 | 39 | 42 | 42 | 36 | 1 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| 12 | 56 | 142 | 34 | 34 | 34 | 34 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| 13 | 59 | 121 | 42 | 43 | 43 | 42 | 1 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| 14 | 60 | 125 | 37 | 38 | 38 | 36 | 1 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| 15 | 61 | 123 | 35 | 36 | 36 | 36 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 16 | 61 | 151 | 31 | 31 | 31 | 31 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| 17 | 69 | 128 | 33 | 33 | 33 | 33 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 18 | 71 | 222 | 31 | 31 | 31 | 31 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 |
| 19 | 72 | 214 | 31 | 31 | 31 | 31 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 |
| 20 | 153 | 15 | 34 | 34 | 34 | 34 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| 21 | 234 | 227 | 41 | 44 | 44 | 38 | 4 | 5 | 7 | 11 | 6 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 22 | 235 | 192 | 36 | 36 | 36 | 36 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| 23 | 236 | 205 | 42 | 44 | 44 | 40 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 |
| 24 | 236 | 194 | 38 | 38 | 38 | 38 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| 25 | 243 | 227 | 37 | 37 | 37 | 37 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 |
| 26 | 245 | 49 | 33 | 33 | 33 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 27 | 249 | 201 | 33 | 33 | 33 | 33 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 |
| 28 | 253 | 152 | 31 | 31 | 31 | 31 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| 29 | 253 | 142 | 37 | 37 | 37 | 37 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| 30 | 256 | 126 | 32 | 34 | 34 | 31 | 1 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| 31 | 257 | 120 | 35 | 37 | 37 | 34 | 1 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| 32 | 263 | 109 | 39 | 41 | 35 | 36 | 1 | 2 | 4 | 11 | 6 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 33 | 276 | 102 | 36 | 36 | 36 | 36 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 34 | 282 | 32 | 34 | 34 | 34 | 34 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 35 | 296 | 66 | 33 | 33 | 33 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 36 | 296 | 90 | 38 | 38 | 38 | 38 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 37 | 290 | 64 | 33 | 36 | 36 | 32 | 0 | 1 | 4 | 11 | 6 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 38 | 291 | 74 | 32 | 32 | 32 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 39 | 293 | 82 | 36 | 37 | 37 | 35 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 40 | 294 | 87 | 40 | 42 | 42 | 37 | 1 | 1 | 2 | 11 | 6 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 41 | 294 | 91 | 36 | 36 | 36 | 36 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 42 | 301 | 62 | 37 | 39 | 35 | 34 | 0 | 1 | 2 | 11 | 6 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 43 | 302 | 64 | 39 | 39 | 39 | 39 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 44 | 302 | 86 | 39 | 39 | 39 | 39 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 45 | 305 | 98 | 33 | 33 | 33 | 33 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 46 | 306 | 52 | 32 | 32 | 32 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 47 | 307 | 66 | 36 | 36 | 36 | 32 | 0 | 1 | 4 | 11 | 6 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 48 | 311 | 31 | 40 | 40 | 40 | 40 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 49 | 313 | 39 | 39 | 40 | 40 | 39 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 50 | 311 | 56 | 32 | 32 | 32 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Table A1. ACDT Volume Scan Output for Volume Scan No. 1, Case Study No. 2
(Cont'd)

| | | | | | | | | | | | | | | | | | | | | | | | | | |
|------|-----|-----|----|----|----|----|---|---|---|------|-----|---|------|------|-----|---|---|-------|------|----|----|----|---|---|---|
| 51 | 312 | 52 | 33 | 34 | 34 | 32 | C | C | 1 | 11.3 | 2.1 | C | 0.00 | 4.7 | 5.0 | C | C | 9.0 | 0.8 | 6 | 30 | 1 | 2 | 1 | |
| 52 | 316 | 25 | 36 | 40 | 40 | 34 | C | C | 1 | 11.3 | 2.1 | C | 0.00 | 2.1 | 1.4 | C | C | 6.8 | 1.3 | 0 | 25 | 0 | 3 | 1 | |
| 53 | 316 | 74 | 38 | 40 | 40 | 34 | C | 2 | 6 | 11.8 | 2.1 | C | 0.08 | 6.1 | 1.9 | C | C | -4.6 | 3.2 | 8 | 19 | 1 | 5 | 1 | |
| 54* | 317 | 42 | 40 | 41 | 40 | 40 | C | 1 | 1 | 11.6 | 2.1 | C | 0.00 | 3.6 | 2.7 | C | C | 10.1 | 3.3 | 7 | 26 | 3 | 3 | 1 | |
| 55 | 318 | 61 | 34 | 35 | 35 | 33 | C | 1 | 1 | 11.3 | 2.1 | C | 0.00 | 5.1 | 3.9 | C | C | 8.5 | 2.1 | 9 | 29 | 0 | 2 | 1 | |
| 56 | 319 | 67 | 35 | 37 | 37 | 34 | C | 1 | 1 | 11.3 | 2.1 | C | 0.00 | 4.7 | 1.6 | C | C | -1.8 | 10.9 | 10 | 19 | 0 | 2 | 1 | |
| 57 | 318 | 91 | 34 | 34 | 34 | 34 | 1 | 1 | 1 | 11.8 | 2.1 | C | 0.00 | 6.1 | 0.0 | C | C | -2.5 | 0.0 | 0 | 31 | 0 | 1 | 1 | |
| 58 | 321 | 80 | 33 | 33 | 33 | 33 | C | 0 | 0 | 11.3 | 2.1 | C | 0.00 | 6.9 | 3.0 | C | C | -1.6 | 3.9 | 6 | 34 | 5 | 1 | 1 | |
| 59 | 322 | 74 | 35 | 35 | 35 | 35 | C | 0 | 0 | 11.3 | 2.1 | C | 0.00 | 2.2 | 1.2 | C | C | -8.0 | 0.9 | 0 | 19 | 1 | 1 | 1 | |
| 60 | 323 | 64 | 33 | 35 | 35 | 32 | 1 | 2 | 5 | 11.3 | 2.1 | C | 0.00 | 3.7 | 1.3 | C | C | -2.3 | 4.1 | 8 | 34 | 1 | 3 | 1 | |
| 61 | 327 | 88 | 37 | 37 | 37 | 37 | 1 | 1 | 1 | 11.6 | 2.1 | C | 0.00 | 1.7 | 0.0 | C | C | -1.8 | 0.0 | 0 | 34 | 0 | 1 | 1 | |
| 62 | 328 | 82 | 33 | 33 | 33 | 33 | 1 | 1 | 1 | 11.3 | 2.1 | C | 0.00 | 3.1 | 1.4 | C | C | -4.7 | 0.4 | 0 | 34 | 2 | 1 | 1 | |
| 63 | 329 | 71 | 42 | 43 | 43 | 43 | C | 0 | 0 | 11.3 | 2.1 | C | 0.00 | 4.9 | 1.3 | C | C | -11.2 | 1.6 | 0 | 19 | 1 | 1 | 1 | |
| 64 | 331 | 65 | 44 | 44 | 44 | 44 | C | 1 | 2 | 11.3 | 2.1 | C | 0.00 | 7.7 | 1.0 | C | C | -12.4 | 1.5 | 11 | 19 | 1 | 1 | 1 | |
| 65* | 334 | 65 | 49 | 45 | 44 | 47 | C | 1 | 4 | 11.6 | 2.1 | C | 0.00 | 6.3 | 3.3 | C | C | -0.5 | 9.0 | 11 | 19 | 4 | 3 | 1 | |
| 66* | 336 | 53 | 53 | 51 | 50 | 49 | C | 2 | 4 | 11.8 | 2.1 | C | 0.00 | 6.1 | 2.7 | C | C | 8.2 | 2.6 | 12 | 19 | 4 | 5 | 1 | |
| 67 | 339 | 86 | 41 | 44 | 44 | 33 | 1 | 1 | 3 | 11.3 | 2.1 | C | 0.00 | 3.2 | 1.6 | C | C | -7.3 | 4.9 | 0 | 34 | 4 | 2 | 1 | |
| 68 | 341 | 95 | 39 | 40 | 40 | 35 | 1 | 1 | 2 | 11.6 | 2.1 | C | 0.00 | 9.4 | 1.4 | C | C | -6.0 | 0.4 | 0 | 34 | 2 | 2 | 1 | |
| 69 | 355 | 51 | 34 | 34 | 34 | 34 | C | 0 | 0 | 11.5 | 2.1 | C | 0.00 | 3.0 | 2.3 | C | C | -2.7 | 8.2 | 13 | 32 | 1 | 1 | 1 | |
| 70 | 337 | 62 | 46 | 47 | 47 | 46 | C | 1 | 1 | 11.3 | 2.1 | C | 0.00 | 4.7 | 3.2 | C | C | -2.0 | 8.3 | 14 | 34 | 4 | 2 | 1 | |
| 71 | 359 | 77 | 42 | 43 | 43 | 43 | C | 0 | 0 | 11.3 | 2.1 | C | 0.00 | 2.9 | 2.5 | C | C | 10.8 | 0.0 | 15 | 34 | 0 | 1 | 1 | |
| 72 | 359 | 73 | 35 | 35 | 35 | 35 | C | 0 | 0 | 11.3 | 2.1 | C | 0.00 | 2.1 | 3.4 | C | C | -5.1 | 0.0 | 15 | 34 | 0 | 1 | 1 | |
| 73 | 359 | 50 | 35 | 35 | 35 | 35 | C | 0 | 0 | 11.3 | 2.1 | C | 0.00 | 1.9 | 0.0 | C | C | -11.4 | 0.0 | 13 | 32 | 0 | 1 | 1 | |
| 74 | 359 | 67 | 37 | 37 | 37 | 37 | C | 0 | 0 | 11.3 | 2.1 | C | 0.00 | 3.2 | 2.8 | C | C | -10.6 | 1.1 | 16 | 34 | 1 | 1 | 1 | |
| 75 | C | 59 | 34 | 36 | 36 | 34 | C | 1 | 3 | 11.3 | 2.1 | C | 0.00 | 3.3 | 1.2 | C | C | -3.4 | 5.2 | 16 | 34 | 0 | 3 | 1 | |
| 76 | 359 | 54 | 32 | 32 | 32 | 32 | C | 2 | 3 | 11.3 | 2.1 | C | 0.00 | 2.0 | 0.0 | C | C | -3.6 | 4.6 | 13 | 33 | 0 | 3 | 1 | |
| 77 | 1 | 61 | 39 | 39 | 39 | 39 | C | 0 | 0 | 11.3 | 2.1 | C | 0.00 | 4.5 | 0.0 | C | C | -12.1 | 0.0 | 16 | 38 | 0 | 1 | 1 | |
| 78 | 1 | 76 | 45 | 45 | 45 | 45 | C | 0 | 0 | 11.3 | 2.1 | C | 0.00 | 6.4 | 5.4 | C | C | 3.0 | 5.9 | 15 | 38 | 2 | 1 | 1 | |
| 79* | 3 | 60 | 40 | 45 | 45 | 33 | C | 1 | 4 | 11.3 | 2.1 | C | 0.00 | 4.5 | 2.5 | C | C | -2.9 | 4.1 | 16 | 38 | 2 | 3 | 1 | |
| 80 | 8 | 67 | 44 | 45 | 45 | 43 | C | 1 | 1 | 11.3 | 2.1 | C | 0.00 | 5.7 | 4.4 | C | C | -2.4 | 3.1 | 16 | 38 | 3 | 2 | 1 | |
| 81* | 12 | 57 | 42 | 45 | 42 | 39 | C | 1 | 4 | 11.3 | 2.1 | C | 0.00 | 4.0 | 1.6 | C | C | -6.7 | 5.6 | 17 | 38 | 2 | 4 | 1 | |
| 82 | 11 | 52 | 40 | 40 | 40 | 40 | C | 0 | 0 | 11.3 | 2.1 | C | 0.00 | 4.1 | 1.5 | C | C | -9.4 | 0.4 | 17 | 38 | 1 | 1 | 1 | |
| 83 | 13 | 44 | 44 | 45 | 43 | 45 | C | 0 | 0 | 11.3 | 2.1 | C | 0.00 | 2.8 | 1.4 | C | C | -1.3 | 6.7 | 0 | 36 | 1 | 2 | 1 | |
| 84 | 18 | 58 | 31 | 31 | 31 | 31 | C | 0 | 0 | 11.3 | 2.1 | C | 0.00 | 2.1 | 3.1 | C | C | -2.0 | 4.7 | 0 | 35 | 2 | 1 | 1 | |
| 85 | 20 | 44 | 33 | 33 | 33 | 33 | C | 0 | 0 | 11.3 | 2.1 | C | 0.00 | 1.8 | 2.4 | C | C | -10.6 | 0.0 | 0 | 37 | 0 | 1 | 1 | |
| 86 | 26 | 95 | 38 | 38 | 38 | 38 | 1 | 1 | 1 | 11.3 | 2.1 | C | 0.00 | 3.3 | 0.0 | C | C | -5.3 | 0.0 | 0 | 39 | 0 | 1 | 1 | |
| 87 | 51 | 101 | 33 | 34 | 33 | 34 | 1 | 1 | 2 | 11.3 | 2.1 | C | 0.00 | 2.1 | 1.1 | C | C | -2.0 | 2.0 | 18 | 5 | 1 | 1 | 1 | |
| 88* | 339 | 56 | 41 | 46 | 34 | 40 | C | 4 | 7 | 11.3 | 2.1 | C | 0.00 | 3.4 | 2.3 | C | C | 5.4 | 3.5 | 12 | 19 | 6 | 4 | 1 | |
| 89 | 344 | 50 | 38 | 40 | 35 | 40 | C | 0 | 0 | 11.3 | 2.1 | C | 0.00 | 2.6 | 2.8 | C | C | 5.4 | 0.7 | 0 | 19 | 2 | 1 | 1 | |
| 91 | 350 | 80 | 34 | 34 | 34 | 34 | C | 0 | 0 | 11.3 | 2.1 | C | 0.00 | 3.0 | 2.4 | C | C | -10.8 | 0.0 | 0 | 34 | 1 | 0 | 1 | |
| 93 | 39 | 81 | 31 | 31 | 31 | 31 | 1 | 1 | 1 | 11.3 | 2.1 | C | 0.00 | 7.6 | 3.3 | C | C | 1.3 | 0.2 | 0 | C | 1 | 1 | 1 | |
| 94 | 40 | 92 | 32 | 32 | 32 | 32 | 2 | 2 | 2 | 11.3 | 2.1 | C | 0.00 | 8.1 | 1.7 | C | C | 5.2 | 0.2 | 0 | C | 1 | 1 | 1 | |
| 95 | 129 | 12 | 33 | 33 | 33 | 33 | C | 0 | 0 | 11.3 | 2.1 | C | 0.00 | 4.7 | 1.0 | C | C | -14.8 | 0.0 | 19 | 0 | 0 | 1 | 1 | |
| 96 | 126 | 17 | 36 | 37 | 36 | 36 | C | 1 | 1 | 11.3 | 2.1 | C | 0.00 | 2.4 | 2.4 | C | C | -1.6 | 8.9 | 19 | 0 | 1 | 4 | 1 | |
| 97 | 228 | 34 | 31 | 31 | 31 | 31 | C | 0 | 0 | 11.3 | 2.1 | C | 0.00 | 1.7 | 1.8 | C | C | -4.8 | 0.0 | 0 | 0 | 0 | 1 | 1 | |
| 98 | 234 | 185 | 33 | 33 | 33 | 33 | 5 | 5 | 5 | 11.3 | 2.1 | C | 0.00 | 30.8 | 0.0 | C | C | C | C | 0 | 0 | 16 | 0 | 1 | 1 |
| 99 | 294 | 61 | 34 | 34 | 34 | 34 | 1 | 1 | 1 | 11.3 | 2.1 | C | 0.00 | 3.0 | 0.0 | C | C | -6.3 | 0.0 | 3 | 19 | 0 | 1 | 1 | |
| 100 | 301 | 80 | 32 | 32 | 32 | 32 | 1 | 1 | 1 | 11.3 | 2.1 | C | 0.00 | 4.0 | 0.0 | C | C | -6.4 | 0.0 | 0 | 0 | 0 | 1 | 1 | |
| 101 | 305 | 61 | 36 | 36 | 36 | 36 | 1 | 1 | 1 | 11.3 | 2.1 | C | 0.00 | 1.9 | 4.3 | C | C | -8.2 | 3.1 | 5 | 19 | 1 | 1 | 1 | |
| 102 | 312 | 68 | 39 | 39 | 35 | 39 | 1 | 1 | 1 | 11.3 | 2.1 | C | 0.00 | 4.0 | 2.4 | C | C | -7.3 | 4.3 | 0 | 19 | 2 | 1 | 1 | |
| 103 | 329 | 17 | 35 | 39 | 31 | 39 | C | 1 | 2 | 11.3 | 2.1 | C | 0.00 | 1.8 | 1.1 | C | C | 9.6 | 1.4 | 0 | C | 0 | 3 | 1 | |
| 104 | 321 | 64 | 32 | 35 | 32 | 32 | 1 | 3 | 5 | 11.3 | 2.1 | C | 0.00 | 2.7 | 2.0 | C | C | 6.8 | 2.7 | 10 | 19 | 0 | 4 | 1 | |
| 105* | 323 | 36 | 44 | 47 | 33 | 47 | C | 2 | 2 | 11.3 | 2.1 | C | 0.00 | 1.9 | 1.8 | C | C | 9.8 | 2.9 | 20 | 26 | 1 | 3 | 1 | |
| 106 | 326 | 40 | 34 | 34 | 34 | 34 | C | 0 | 0 | 11.3 | 2.1 | C | 0.00 | 1.5 | 1.4 | C | C | 9.7 | 2.1 | 20 | 26 | 2 | 1 | 1 | |

Table A1. ACCT Volume Scan Output for Volume Scan No. 1, Case Study No. 2
(Cont D)

| | | | | | | | | | | | | | | | | | | | | | | |
|-----|-----|-----|----|----|----|----|---|---|---|------|-----|------|------|-----|-----|-------|-----|----|----|---|---|---|
| 107 | 330 | 63 | 76 | 39 | 39 | 31 | 1 | 2 | 4 | 11.8 | 2.1 | 0.00 | 7.8 | 1.4 | 0.0 | -4.9 | 3.1 | 0 | 34 | 2 | 2 | 1 |
| 108 | 333 | 75 | 35 | 32 | 35 | 31 | 1 | 1 | 4 | 11.8 | 2.1 | 0.00 | 5.2 | 1.1 | 0.0 | -1.7 | 7.9 | 0 | 19 | 0 | 4 | 1 |
| 109 | 344 | 85 | 31 | 31 | 31 | 31 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 7.5 | 1.6 | 0.0 | -0.6 | 0.1 | 0 | 0 | 1 | 1 | 1 |
| 110 | 350 | 89 | 32 | 42 | 40 | 33 | 2 | 2 | 3 | 11.8 | 2.1 | 0.00 | 3.5 | 2.0 | 0.0 | -4.9 | 1.5 | 0 | 36 | 1 | 2 | 1 |
| 111 | 352 | 57 | 32 | 32 | 31 | 32 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.2 | 0.0 | 0.0 | 3.9 | 0.0 | 0 | 0 | 0 | 1 | 1 |
| 112 | 352 | 58 | 38 | 42 | 42 | 36 | 1 | 1 | 3 | 11.8 | 2.1 | 0.00 | 4.2 | 3.2 | 0.0 | -1.4 | 7.0 | 1 | 38 | 3 | 2 | 1 |
| 113 | 352 | 57 | 36 | 39 | 39 | 33 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 5.1 | 3.0 | 0.0 | -0.1 | 4.6 | 0 | 28 | 4 | 0 | 1 |
| 114 | 352 | 57 | 31 | 42 | 42 | 38 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 3.5 | 3.7 | 0.0 | -2.2 | 6.4 | 1 | 38 | 3 | 2 | 1 |
| 115 | 12 | 62 | 40 | 40 | 40 | 41 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 6.0 | 0.3 | 0.0 | -5.0 | 5.2 | 17 | 39 | 4 | 1 | 1 |
| 116 | 52 | 106 | 32 | 32 | 32 | 32 | 1 | 1 | 2 | 11.8 | 2.1 | 0.00 | 2.2 | 0.0 | 0.0 | -0.0 | 0.0 | 18 | 5 | 2 | 1 | 1 |
| 120 | 55 | 116 | 33 | 33 | 33 | 33 | 1 | 1 | 3 | 11.8 | 2.1 | 0.00 | 4.9 | 0.0 | 0.0 | -4.7 | 0.0 | 0 | 0 | 0 | 1 | 1 |
| 121 | 156 | 35 | 32 | 34 | 31 | 34 | 1 | 1 | 3 | 11.8 | 2.1 | 0.00 | 2.5 | 5.0 | 0.0 | -2.1 | 3.3 | 0 | 0 | 2 | 3 | 1 |
| 122 | 265 | 104 | 33 | 35 | 35 | 32 | 4 | 1 | 6 | 11.8 | 2.1 | 0.00 | 3.4 | 0.0 | 0.0 | -0.9 | 1.3 | 0 | 23 | 0 | 2 | 1 |
| 123 | 319 | 56 | 77 | 38 | 38 | 34 | 2 | 1 | 5 | 11.8 | 2.1 | 0.00 | 3.6 | 5.2 | 0.0 | -5.5 | 3.8 | 9 | 29 | 3 | 4 | 1 |
| 124 | 321 | 45 | 36 | 33 | 34 | 35 | 1 | 4 | 3 | 11.8 | 2.1 | 0.00 | 0.8 | 4.7 | 0.0 | -6.5 | 5.4 | 21 | 26 | 2 | 5 | 1 |
| 125 | 321 | 30 | 42 | 42 | 42 | 43 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 3.1 | 1.5 | 0.0 | -10.4 | 1.1 | 20 | 26 | 0 | 2 | 1 |
| 126 | 337 | 69 | 41 | 44 | 44 | 34 | 2 | 4 | 7 | 11.8 | 2.1 | 0.00 | 5.4 | 1.3 | 0.0 | -2.7 | 0.7 | 22 | 19 | 1 | 3 | 1 |
| 127 | 340 | 64 | 43 | 45 | 45 | 43 | 2 | 1 | 1 | 11.8 | 2.1 | 0.00 | 2.5 | 1.4 | 0.0 | -1.1 | 1.8 | 23 | 19 | 2 | 3 | 1 |
| 128 | 347 | 61 | 31 | 31 | 31 | 31 | 2 | 2 | 3 | 11.8 | 2.1 | 0.00 | 0.1 | 1.1 | 0.0 | -0.4 | 0.9 | 24 | 0 | 1 | 2 | 1 |
| 129 | 352 | 83 | 31 | 31 | 31 | 31 | 1 | 4 | 5 | 11.8 | 2.1 | 0.00 | 8.8 | 0.0 | 0.0 | -1.5 | 1.0 | 0 | 0 | 0 | 2 | 1 |
| 130 | 12 | 76 | 35 | 37 | 37 | 33 | 1 | 4 | 6 | 11.8 | 2.1 | 0.00 | 1.9 | 1.7 | 0.0 | -4.6 | 0.1 | 16 | 38 | 0 | 3 | 1 |
| 131 | 319 | 78 | 35 | 32 | 32 | 35 | 1 | 4 | 6 | 11.8 | 2.1 | 0.00 | 4.1 | 4.1 | 0.0 | -1.7 | 4.5 | 8 | 34 | 4 | 3 | 1 |
| 132 | 352 | 57 | 38 | 30 | 38 | 38 | 1 | 3 | 1 | 11.8 | 2.1 | 0.00 | 3.0 | 1.2 | 0.0 | -1.3 | 0.5 | 16 | 38 | 1 | 1 | 1 |
| 133 | 334 | 27 | 32 | 33 | 32 | 33 | 1 | 2 | 4 | 11.8 | 2.1 | 0.00 | 2.1 | 1.1 | 0.0 | -7.1 | 1.4 | 20 | 26 | 0 | 4 | 1 |
| 134 | 328 | 34 | 40 | 43 | 40 | 41 | 2 | 4 | 7 | 11.8 | 2.1 | 0.00 | 0.3 | 2.2 | 0.0 | -8.3 | 2.7 | 20 | 26 | 2 | 6 | 1 |
| 135 | 316 | 49 | 34 | 34 | 34 | 34 | 2 | 0 | 7 | 11.8 | 2.1 | 0.00 | 1.4 | 4.4 | 0.0 | -8.6 | 0.0 | 21 | 26 | 0 | 1 | 1 |
| 136 | 325 | 29 | 36 | 36 | 36 | 36 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.7 | 0.0 | 0.0 | -10.5 | 0.0 | 20 | 26 | 0 | 1 | 1 |
| 137 | 20 | 49 | 37 | 37 | 37 | 37 | 1 | 1 | 2 | 11.8 | 2.1 | 0.00 | 0.5 | 1.8 | 0.0 | -1.1 | 0.4 | 0 | 0 | 1 | 1 | 1 |
| 138 | 347 | 55 | 33 | 34 | 34 | 32 | 4 | 5 | 5 | 11.8 | 2.1 | 0.00 | 0.5 | 1.0 | 0.0 | -1.2 | 0.3 | 24 | 19 | 0 | 2 | 1 |
| 139 | 13 | 62 | 35 | 37 | 37 | 33 | 5 | 4 | 7 | 11.8 | 2.1 | 0.00 | 3.7 | 1.6 | 0.0 | -5.2 | 0.5 | 16 | 38 | 2 | 2 | 1 |
| 140 | 14 | 67 | 36 | 36 | 36 | 36 | 5 | 5 | 5 | 11.8 | 2.1 | 0.00 | 1.6 | 1.7 | 0.0 | -6.3 | 0.0 | 16 | 38 | 0 | 1 | 1 |
| 141 | 16 | 61 | 42 | 44 | 44 | 40 | 5 | 5 | 6 | 11.8 | 2.1 | 0.00 | -1.1 | 2.2 | 0.0 | -5.0 | 2.5 | 0 | 28 | 2 | 2 | 1 |
| 142 | 334 | 68 | 34 | 34 | 34 | 34 | 5 | 5 | 5 | 11.8 | 2.1 | 0.00 | 1.9 | 1.4 | 0.0 | -4.7 | 0.0 | 22 | 19 | 0 | 1 | 1 |
| 143 | 341 | 63 | 36 | 36 | 36 | 36 | 5 | 5 | 5 | 11.8 | 2.1 | 0.00 | 1.5 | 0.0 | 0.0 | -0.5 | 0.0 | 23 | 19 | 0 | 1 | 1 |
| 144 | 15 | 73 | 33 | 33 | 33 | 33 | 6 | 6 | 6 | 11.8 | 2.1 | 0.00 | 4.7 | 1.0 | 0.0 | -5.5 | 0.0 | 16 | 38 | 0 | 1 | 1 |
| 145 | 325 | 47 | 34 | 35 | 35 | 32 | 4 | 5 | 6 | 11.8 | 2.1 | 0.00 | 3.5 | 1.6 | 0.0 | -11.1 | 0.7 | 21 | 26 | 0 | 2 | 1 |
| 146 | 340 | 51 | 37 | 37 | 37 | 37 | 6 | 6 | 6 | 11.8 | 2.1 | 0.00 | 3.0 | 4.6 | 0.0 | -5.7 | 1.7 | 0 | 19 | 2 | 1 | 1 |
| 147 | 344 | 18 | 35 | 37 | 34 | 36 | 2 | 3 | 7 | 11.8 | 2.1 | 0.00 | 1.9 | 1.4 | 0.0 | -5.3 | 1.0 | 0 | 0 | 0 | 3 | 1 |
| 148 | 325 | 40 | 39 | 39 | 39 | 39 | 8 | 8 | 8 | 11.8 | 2.1 | 0.00 | 2.8 | 3.9 | 0.0 | -0.9 | 0.0 | 0 | 26 | 0 | 1 | 1 |

Table A1: ACDT Volume Scan Output for Volume Scan No. 1, Case Study No. 2 (Contd)

| CLUSTER OUTPUT | | | | | | | | | | | | | | | | | | | | | | | |
|---|------|-------|------|------|------|-----|-----|-----|------|------|------|------|-----|----|----|------|------|----|---|---|---|---|--|
| CENTROID | | | | | | | | | | | | | | | | | | | | | | | |
| TRK | AZM | RNG | AV | PK | V | X | L | AN | IC | AV | CELL | MSKM | MT | IC | IC | RCT | DIV | RC | | | | | |
| NO | DEG | KM | 50 | 50 | C | KM | AM | 50 | | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | | | | | |
| 1 | 60 | 125 | 39 | 43 | 2 | 0.0 | 3.6 | 53 | 10 | 0.0 | 0.0 | 0.7 | 5 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 2 | 257 | 123 | 34 | 37 | 2 | 0.0 | 0.0 | 0 | 21 | 0.0 | 0.0 | 0.0 | 3 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 3 | 290 | 63 | 33 | 36 | 2 | 0.0 | 3.6 | 47 | 15 | 0.0 | 0.0 | 0.5 | 4 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 4 | 293 | 87 | 37 | 42 | 2 | 0.0 | 3.6 | 102 | 1 | 0.0 | 0.0 | 1.0 | 2 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 5 | 303 | 62 | 37 | 39 | 2 | 1.1 | 2.5 | 54 | 19 | 0.0 | 0.0 | 1.9 | 2 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 6 | 310 | 53 | 32 | 34 | 2 | 1.6 | 2.3 | 37 | 30 | 0.0 | 0.0 | 4.5 | 1 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 7 | 315 | 40 | 39 | 41 | 2 | 0.0 | 0.0 | 0 | 24 | 0.0 | 0.0 | 2.3 | 1 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 8 | 320 | 79 | 36 | 40 | 4 | 0.0 | 5.2 | 6 | 15 | 0.0 | 0.0 | 2.8 | 6 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 9 | 318 | 53 | 35 | 38 | 2 | 0.0 | 1.0 | 0 | 24 | 0.0 | 0.0 | 4.5 | 5 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 10 | 320 | 66 | 34 | 37 | 2 | 0.0 | 0.0 | 0 | 15 | 0.0 | 0.0 | 1.9 | 5 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 11 | 332 | 65 | 43 | 45 | 2 | 0.0 | 0.0 | 0 | 15 | 0.0 | 0.0 | 2.4 | 4 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 12 | 333 | 54 | 47 | 51 | 2 | 0.0 | 0.0 | 0 | 15 | 0.0 | 0.0 | 2.6 | 7 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 13 | 358 | 51 | 33 | 35 | 2 | 1.0 | 1.9 | 46 | 32 | 0.0 | 0.0 | 0.9 | 3 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 14 | 353 | 83 | 44 | 47 | 2 | 0.0 | 0.0 | 0 | 34 | 0.0 | 0.0 | 2.2 | 3 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 15 | 0 | 75 | 42 | 45 | 2 | 1.0 | 1.7 | 36 | 36 | 0.0 | 0.0 | 4.2 | 0 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 16 | 0 | 63 | 38 | 40 | 11 | 3.4 | 7.4 | 55 | 31 | 0.0 | 0.0 | 2.7 | 7 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 17 | 12 | 57 | 40 | 45 | 2 | 0.4 | 4.1 | 15 | 31 | 0.0 | 0.0 | 1.9 | 4 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 18 | 52 | 103 | 32 | 34 | 2 | 0.0 | 0.0 | 0 | 5 | 0.0 | 0.0 | 0.6 | 2 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 19 | 127 | 15 | 34 | 37 | 2 | 0.0 | 0.0 | 0 | 0 | 0.0 | 0.0 | 2.0 | 1 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 20 | 326 | 33 | 40 | 47 | 2 | 1.5 | 4.9 | 314 | 26 | 0.0 | 0.0 | 1.6 | 7 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 21 | 321 | 47 | 34 | 38 | 2 | 1.1 | 0.5 | 53 | 26 | 0.0 | 0.0 | 2.9 | 6 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 22 | 335 | 63 | 39 | 44 | 2 | 0.0 | 0.0 | 0 | 19 | 0.0 | 0.0 | 1.3 | 7 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 23 | 340 | 64 | 41 | 45 | 2 | 0.0 | 0.0 | 0 | 19 | 0.0 | 0.0 | 1.2 | 5 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| 24 | 347 | 58 | 32 | 34 | 2 | 0.0 | 0.0 | 0 | 19 | 0.0 | 0.0 | 1.0 | 5 | 0 | 0 | 0.00 | 0.00 | 0 | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | |
| VOL HMM AREA WFLX NEAR NEIGHBOR ACT NO NO VELOCITY TRK CLS CNT G OVER | | | | | | | | | | | | | | | | | | | | | | | |
| SCAN | KMM2 | KMT/H | CELL | CLST | CONT | VCL | CS | FC | EM/S | NP/S | NC | CTR | CTR | C | | | | | | | | | |
| 1 | 1534 | 5.0 | 27.0 | 7.0 | 13.0 | 0.0 | 143 | 25 | 13 | 11.8 | 2.1 | 148 | 24 | 39 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |

Table A2. ACDT Volume Scan Output for Volume Scan No. 2, Case Study No. 2

| SCAN TIME 100 154044 - 154703 | | | | | | | | | | VOL SCAN 2 AZ = 71.1 TD 70.6 (DEG) | | | | | | | | | | | |
|--------------------------------|-----|-----|-----|-----|----|----|----|---|---|-------------------------------------|------|-----|-------|------|-----|------|------|----|----|----|--|
| TRACK REF TIME 101930 - 154044 | | | | | | | | | | AZM SCAN 10/1 EL = 0.0 TD 6.5 (DEG) | | | | | | | | | | | |
| FIXED CONTIGUR OUTPUT | | | | | | | | | | | | | | | | | | | | | |
| CENTROID AV CELL 2 | | | | | | | | | | WTR AREA VELOCITY NEAR MX MR SP | | | | | | | | | | | |
| TRK | AZM | RNG | AZM | RNG | AV | PK | V | D | A | SPR | PRE | D | FLUX | ACCN | AV | CELL | DIST | HT | IC | IC | |
| NO | DEG | KM | DEG | KM | CH | DE | C | C | L | KM | KM | I | M/T/H | K/M2 | DEG | M/S | KM | NO | NO | NO | |
| 40 | 100 | 16 | 100 | 15 | 35 | 35 | 2 | 0 | 0 | 0.0 | 0.0 | 0 | 0.05 | 0.01 | 217 | 19 | 0.0 | 0 | 0 | 0 | |
| 17 | 242 | 194 | 242 | 194 | 31 | 31 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.02 | 0.01 | 258 | 19 | 0.0 | 4 | 0 | 0 | |
| 41 | 161 | 31 | 159 | 30 | 36 | 38 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.06 | 0.01 | 999 | 999 | 0.0 | 1 | 0 | 0 | |
| 42 | 147 | 33 | 144 | 32 | 31 | 32 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.03 | 0.01 | 999 | 999 | 0.0 | 1 | 0 | 0 | |
| 16 | 236 | 194 | 236 | 184 | 39 | 45 | 4 | 1 | 0 | 1.4 | 10.4 | 49 | 3.18 | 0.53 | 135 | 16 | 0.0 | 7 | 0 | 0 | |
| 43 | 259 | 118 | 260 | 116 | 32 | 33 | 2 | 0 | 0 | 0.0 | 0.0 | 0 | 0.21 | 0.07 | 999 | 999 | 0.0 | 2 | 0 | 0 | |
| 44 | 240 | 26 | 242 | 24 | 33 | 35 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.02 | 0.01 | 999 | 999 | 0.0 | 0 | 0 | 0 | |
| 15 | 233 | 21 | 232 | 219 | 43 | 48 | 2 | 1 | 0 | 0.0 | 0.0 | 0 | 4.57 | 0.44 | 249 | 14 | 0.0 | 9 | 0 | 0 | |
| 45 | 242 | 226 | 242 | 227 | 37 | 38 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.42 | 0.09 | 999 | 999 | 0.0 | 6 | 0 | 0 | |
| 46 | 244 | 217 | 244 | 217 | 31 | 31 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.25 | 0.04 | 999 | 999 | 0.0 | 5 | 0 | 0 | |
| 47 | 252 | 158 | 251 | 159 | 36 | 37 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.40 | 0.12 | 999 | 999 | 0.0 | 4 | 0 | 0 | |
| 48 | 253 | 146 | 255 | 146 | 32 | 32 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.07 | 0.03 | 999 | 999 | 0.0 | 2 | 0 | 0 | |
| 49 | 274 | 71 | 276 | 70 | 31 | 32 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.02 | 0.01 | 999 | 999 | 0.0 | 3 | 0 | 0 | |
| 23 | 269 | 103 | 268 | 102 | 37 | 46 | 5 | 2 | 1 | 2.4 | 8.3 | 28 | 1.41 | 0.37 | 215 | 22 | 0.1 | 6 | 0 | 0 | |
| 50 | 271 | 92 | 272 | 92 | 30 | 34 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.02 | 0.01 | 999 | 999 | 0.0 | 1 | 0 | 0 | |
| 51 | 280 | 75 | 280 | 75 | 31 | 31 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.02 | 0.01 | 999 | 999 | 0.0 | 1 | 0 | 0 | |
| 52 | 286 | 92 | 286 | 91 | 32 | 32 | 0 | 0 | 0 | 0.0 | 0.0 | 0 | 0.06 | 0.02 | 225 | 14 | 0.0 | 1 | 0 | 3 | |
| 53 | 280 | 73 | 281 | 77 | 34 | 35 | 1 | 1 | 1 | 0.0 | 0.0 | 0 | 0.03 | 0.01 | 999 | 999 | 0.0 | 1 | 0 | 0 | |
| 26 | 312 | 26 | 312 | 25 | 38 | 38 | 1 | 1 | 1 | 0.0 | 0.0 | 0 | 0.03 | 0.01 | 102 | 17 | 0.0 | 0 | 0 | 0 | |
| 3 | 290 | 82 | 299 | 88 | 36 | 41 | 5 | 1 | 1 | 8.1 | 7.7 | 35 | 1.75 | 0.43 | 238 | 16 | 0.2 | 2 | 24 | 0 | |
| 54 | 303 | 76 | 304 | 76 | 33 | 34 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.02 | 0.01 | 262 | 15 | 0.0 | 1 | 0 | 0 | |
| 55 | 311 | 99 | 311 | 99 | 34 | 34 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.04 | 0.01 | 999 | 999 | 0.0 | 1 | 0 | 0 | |
| 56 | 341 | 67 | 343 | 69 | 41 | 52 | 14 | 4 | 4 | 5.1 | 7.7 | 117 | 1.96 | 0.26 | 257 | 15 | 4.0 | 6 | 19 | 34 | |
| 57 | 322 | 81 | 323 | 81 | 31 | 31 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.02 | 0.01 | 252 | 23 | 0.0 | 1 | 0 | 34 | |
| 58 | 359 | 32 | 359 | 63 | 34 | 34 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.05 | 0.01 | 999 | 999 | 0.0 | 0 | 0 | 0 | |
| 57 | 356 | 92 | 348 | 93 | 41 | 45 | 6 | 3 | 2 | 3.3 | 11.6 | 229 | 2.05 | 0.27 | 263 | 21 | 0.2 | 3 | 0 | 34 | |
| 34 | 321 | 60 | 323 | 60 | 39 | 48 | 31 | 3 | 3 | 9.9 | 14.4 | 310 | 3.48 | 0.61 | 246 | 13 | 4.1 | 7 | 19 | 0 | |
| 60 | 333 | 91 | 332 | 92 | 35 | 37 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.12 | 0.03 | 999 | 999 | 0.0 | 2 | 0 | 0 | |
| 19 | 338 | 53 | 337 | 54 | 26 | 36 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.01 | 0.00 | 177 | 6 | 0.0 | 5 | 0 | 0 | |
| 61 | 2 | 63 | 2 | 63 | 32 | 32 | 1 | 1 | 1 | 0.0 | 0.0 | 0 | 0.03 | 0.02 | 200 | 13 | 0.0 | 0 | 0 | 34 | |
| 62 | 33 | 99 | 34 | 95 | 35 | 37 | 2 | 0 | 0 | 0.0 | 0.0 | 0 | 0.28 | 0.08 | 999 | 999 | 0.0 | 1 | 0 | 0 | |
| 63 | 9 | 74 | 12 | 73 | 39 | 45 | 12 | 2 | 1 | 3.5 | 11.9 | 230 | 3.71 | 0.50 | 250 | 14 | 0.2 | 6 | 38 | 34 | |
| 64 | 48 | 113 | 49 | 114 | 32 | 34 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.03 | 0.01 | 999 | 999 | 0.0 | 3 | 0 | 0 | |
| 65 | 51 | 135 | 51 | 134 | 39 | 38 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.27 | 0.06 | 999 | 999 | 0.0 | 2 | 0 | 0 | |
| 66 | 52 | 122 | 52 | 122 | 31 | 32 | 1 | 1 | 1 | 0.0 | 0.0 | 0 | 0.01 | 0.01 | 999 | 999 | 0.0 | 7 | 0 | 0 | |
| 67 | 52 | 132 | 52 | 132 | 35 | 42 | 1 | 1 | 1 | 0.0 | 0.0 | 0 | 0.57 | 0.09 | 999 | 999 | 0.0 | 8 | 0 | 0 | |
| 10 | 59 | 121 | 60 | 121 | 35 | 35 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.07 | 0.02 | 327 | 4 | 0.0 | 2 | 0 | 0 | |

Table A2. ACPI Volume Scan Output for Volume Scan No. 2, Case Study No. 2
(continued)

| ACPI Volume Scan Output | | Volume Scan No. 2 | | Case Study No. 2 | |
|-------------------------|------|-------------------|------|------------------|------|
| Line | Time | Time | Time | Time | Time |
| 101 | 101 | 101 | 101 | 101 | 101 |
| 102 | 102 | 102 | 102 | 102 | 102 |
| 103 | 103 | 103 | 103 | 103 | 103 |
| 104 | 104 | 104 | 104 | 104 | 104 |
| 105 | 105 | 105 | 105 | 105 | 105 |
| 106 | 106 | 106 | 106 | 106 | 106 |
| 107 | 107 | 107 | 107 | 107 | 107 |
| 108 | 108 | 108 | 108 | 108 | 108 |
| 109 | 109 | 109 | 109 | 109 | 109 |
| 110 | 110 | 110 | 110 | 110 | 110 |
| 111 | 111 | 111 | 111 | 111 | 111 |
| 112 | 112 | 112 | 112 | 112 | 112 |
| 113 | 113 | 113 | 113 | 113 | 113 |
| 114 | 114 | 114 | 114 | 114 | 114 |
| 115 | 115 | 115 | 115 | 115 | 115 |
| 116 | 116 | 116 | 116 | 116 | 116 |
| 117 | 117 | 117 | 117 | 117 | 117 |
| 118 | 118 | 118 | 118 | 118 | 118 |
| 119 | 119 | 119 | 119 | 119 | 119 |
| 120 | 120 | 120 | 120 | 120 | 120 |
| 121 | 121 | 121 | 121 | 121 | 121 |
| 122 | 122 | 122 | 122 | 122 | 122 |
| 123 | 123 | 123 | 123 | 123 | 123 |
| 124 | 124 | 124 | 124 | 124 | 124 |
| 125 | 125 | 125 | 125 | 125 | 125 |
| 126 | 126 | 126 | 126 | 126 | 126 |
| 127 | 127 | 127 | 127 | 127 | 127 |
| 128 | 128 | 128 | 128 | 128 | 128 |
| 129 | 129 | 129 | 129 | 129 | 129 |
| 130 | 130 | 130 | 130 | 130 | 130 |
| 131 | 131 | 131 | 131 | 131 | 131 |
| 132 | 132 | 132 | 132 | 132 | 132 |
| 133 | 133 | 133 | 133 | 133 | 133 |
| 134 | 134 | 134 | 134 | 134 | 134 |
| 135 | 135 | 135 | 135 | 135 | 135 |
| 136 | 136 | 136 | 136 | 136 | 136 |
| 137 | 137 | 137 | 137 | 137 | 137 |
| 138 | 138 | 138 | 138 | 138 | 138 |
| 139 | 139 | 139 | 139 | 139 | 139 |
| 140 | 140 | 140 | 140 | 140 | 140 |
| 141 | 141 | 141 | 141 | 141 | 141 |
| 142 | 142 | 142 | 142 | 142 | 142 |
| 143 | 143 | 143 | 143 | 143 | 143 |
| 144 | 144 | 144 | 144 | 144 | 144 |
| 145 | 145 | 145 | 145 | 145 | 145 |
| 146 | 146 | 146 | 146 | 146 | 146 |
| 147 | 147 | 147 | 147 | 147 | 147 |
| 148 | 148 | 148 | 148 | 148 | 148 |
| 149 | 149 | 149 | 149 | 149 | 149 |
| 150 | 150 | 150 | 150 | 150 | 150 |
| 151 | 151 | 151 | 151 | 151 | 151 |
| 152 | 152 | 152 | 152 | 152 | 152 |
| 153 | 153 | 153 | 153 | 153 | 153 |
| 154 | 154 | 154 | 154 | 154 | 154 |
| 155 | 155 | 155 | 155 | 155 | 155 |
| 156 | 156 | 156 | 156 | 156 | 156 |
| 157 | 157 | 157 | 157 | 157 | 157 |
| 158 | 158 | 158 | 158 | 158 | 158 |
| 159 | 159 | 159 | 159 | 159 | 159 |
| 160 | 160 | 160 | 160 | 160 | 160 |
| 161 | 161 | 161 | 161 | 161 | 161 |
| 162 | 162 | 162 | 162 | 162 | 162 |
| 163 | 163 | 163 | 163 | 163 | 163 |
| 164 | 164 | 164 | 164 | 164 | 164 |
| 165 | 165 | 165 | 165 | 165 | 165 |
| 166 | 166 | 166 | 166 | 166 | 166 |
| 167 | 167 | 167 | 167 | 167 | 167 |
| 168 | 168 | 168 | 168 | 168 | 168 |
| 169 | 169 | 169 | 169 | 169 | 169 |
| 170 | 170 | 170 | 170 | 170 | 170 |
| 171 | 171 | 171 | 171 | 171 | 171 |
| 172 | 172 | 172 | 172 | 172 | 172 |
| 173 | 173 | 173 | 173 | 173 | 173 |
| 174 | 174 | 174 | 174 | 174 | 174 |
| 175 | 175 | 175 | 175 | 175 | 175 |
| 176 | 176 | 176 | 176 | 176 | 176 |
| 177 | 177 | 177 | 177 | 177 | 177 |
| 178 | 178 | 178 | 178 | 178 | 178 |
| 179 | 179 | 179 | 179 | 179 | 179 |
| 180 | 180 | 180 | 180 | 180 | 180 |
| 181 | 181 | 181 | 181 | 181 | 181 |
| 182 | 182 | 182 | 182 | 182 | 182 |
| 183 | 183 | 183 | 183 | 183 | 183 |
| 184 | 184 | 184 | 184 | 184 | 184 |
| 185 | 185 | 185 | 185 | 185 | 185 |
| 186 | 186 | 186 | 186 | 186 | 186 |
| 187 | 187 | 187 | 187 | 187 | 187 |
| 188 | 188 | 188 | 188 | 188 | 188 |
| 189 | 189 | 189 | 189 | 189 | 189 |
| 190 | 190 | 190 | 190 | 190 | 190 |
| 191 | 191 | 191 | 191 | 191 | 191 |
| 192 | 192 | 192 | 192 | 192 | 192 |
| 193 | 193 | 193 | 193 | 193 | 193 |
| 194 | 194 | 194 | 194 | 194 | 194 |
| 195 | 195 | 195 | 195 | 195 | 195 |
| 196 | 196 | 196 | 196 | 196 | 196 |
| 197 | 197 | 197 | 197 | 197 | 197 |
| 198 | 198 | 198 | 198 | 198 | 198 |
| 199 | 199 | 199 | 199 | 199 | 199 |
| 200 | 200 | 200 | 200 | 200 | 200 |

Table A-1. ACPL-1000 P-1000 Optimization Example, Case No. 2, Case Study No. 2

| | | | | | | | | | | | | | | | | | | | | | |
|------|----|----|----|----|----|----|---|---|------|-----|------|-----|-----|------|------|-----|----|----|---|---|---|
| 114 | 11 | 74 | 42 | 43 | 43 | 43 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -2.8 | 7.3 | 16 | 63 | 1 | 1 | 2 |
| 115* | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -0.9 | 6.6 | 16 | 63 | 4 | 4 | 1 |
| 116 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 3.7 | 0.9 | 0 | 23 | 2 | 0 | 2 |
| 117 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 12.6 | 2.5 | 25 | 34 | 1 | 2 | 2 |
| 118* | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 4.7 | 3.4 | 25 | 34 | 4 | 3 | 2 |
| 119* | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -1.6 | 8.3 | 22 | 56 | 3 | 3 | 2 |
| 120* | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 4.1 | 4.5 | 12 | 56 | 5 | 2 | 2 |
| 121 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 8.9 | 0.0 | 0 | 0 | 1 | 0 | 2 |
| 122 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -2.4 | 2.7 | 0 | 63 | 1 | 1 | 2 |
| 123 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 6.1 | 0.0 | 16 | 63 | 1 | 0 | 2 |
| 124* | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -4.9 | 5.0 | 25 | 34 | 8 | 7 | 1 |
| 125 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -3.1 | 2.8 | 16 | 63 | 2 | 1 | 2 |
| 126 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 6.4 | 4.1 | 29 | 26 | 0 | 3 | 2 |
| 127 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 4.6 | 3.8 | 26 | 34 | 2 | 2 | 2 |
| 128* | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -0.8 | 5.7 | 16 | 63 | 5 | 4 | 1 |
| 129* | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -2.9 | 2.2 | 16 | 63 | 3 | 4 | 1 |
| 130 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -2.7 | 1.1 | 16 | 63 | 2 | 4 | 1 |
| 131 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 1.2 | 4.2 | 12 | 56 | 3 | 0 | 2 |
| 132 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -4.4 | 0.0 | 0 | 63 | 1 | 0 | 2 |
| 133* | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 8.2 | 1.0 | 22 | 34 | 2 | 3 | 2 |
| 134 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 14.4 | 0.0 | 0 | 40 | 0 | 1 | 1 |
| 135 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -2.3 | 8.7 | 0 | 42 | 0 | 4 | 1 |
| 136 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -5.1 | 4.9 | 0 | 41 | 1 | 3 | 1 |
| 137 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -1.0 | 5.0 | 0 | 16 | 0 | 1 | 1 |
| 138* | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -0.7 | 9.3 | 0 | 44 | 0 | 4 | 1 |
| 139 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -1.8 | 0.3 | 0 | 45 | 0 | 2 | 1 |
| 140 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -0.7 | 0.0 | 0 | 46 | 0 | 1 | 1 |
| 141* | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -0.3 | 0.1 | 0 | 47 | 0 | 2 | 1 |
| 142 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -0.3 | 0.0 | 0 | 48 | 0 | 1 | 1 |
| 143 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -4.2 | 0.2 | 0 | 43 | 2 | 2 | 1 |
| 144 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 1.3 | 0.2 | 0 | 43 | 0 | 2 | 1 |
| 145 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -0.8 | 1.1 | 32 | 56 | 0 | 2 | 1 |
| 146 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 1.0 | 1.2 | 30 | 23 | 0 | 3 | 1 |
| 147 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 0.7 | 0.4 | 32 | 23 | 0 | 2 | 1 |
| 148 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 1.5 | 3.3 | 0 | 49 | 0 | 3 | 1 |
| 149 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -7.2 | 0.5 | 31 | 93 | 0 | 2 | 1 |
| 150 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -1.8 | 0.0 | 31 | 51 | 0 | 1 | 1 |
| 151 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -0.9 | 0.0 | 0 | 52 | 0 | 1 | 1 |
| 152 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -0.1 | 0.0 | 0 | 3 | 0 | 1 | 1 |
| 153 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 1.2 | 0.0 | 0 | 3 | 0 | 1 | 1 |
| 154 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -0.1 | 0.0 | 0 | 3 | 0 | 1 | 1 |
| 155 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 1.2 | 0.0 | 0 | 3 | 0 | 1 | 1 |
| 156 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 0.9 | 0.0 | 0 | 55 | 0 | 1 | 1 |
| 157 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 5.5 | 2.0 | 25 | 34 | 1 | 2 | 1 |
| 158 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 0.3 | 0.7 | 0 | 60 | 0 | 2 | 1 |
| 159 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -2.3 | 2.0 | 32 | 59 | 2 | 3 | 1 |
| 160 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 0.9 | 0.0 | 0 | 59 | 0 | 1 | 1 |
| 161 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -2.9 | 2.1 | 32 | 59 | 3 | 3 | 1 |
| 162 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -3.0 | 3.9 | 0 | 59 | 2 | 3 | 1 |
| 163 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 3.3 | 5.4 | 33 | 59 | 4 | 3 | 1 |
| 164* | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -1.7 | 7.9 | 33 | 63 | 3 | 4 | 1 |
| 165 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -3.6 | 0.7 | 0 | 62 | 1 | 3 | 1 |
| 166 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 2.5 | 0.0 | 0 | 62 | 0 | 1 | 1 |
| 167 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 3.2 | 0.5 | 0 | 64 | 0 | 2 | 1 |
| 168 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -1.6 | 1.8 | 0 | 63 | 1 | 1 | 1 |
| 169 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 1.4 | 1.2 | 34 | 64 | 0 | 4 | 1 |
| 170 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | 2.7 | 2.1 | 0 | 67 | 2 | 4 | 1 |
| 171 | 11 | 74 | 41 | 44 | 44 | 44 | 1 | 1 | 11.3 | 5.7 | 1.00 | 5.9 | 2.2 | C.C. | -1.9 | 0.1 | 4 | 3 | 2 | 1 | 4 |

Table A2. ACPT Volume Scan Output for Volume Scan No. 2, Case Study No. 2
(Cont'd)

| | | | | | | | | | | | | | | | | | | | | | |
|-----|-----|-----|----|----|----|---|---|---|------|-----|------|-----|-----|-----|------|-----|----|----|---|---|---|
| 185 | 165 | 41 | 34 | 34 | 34 | 0 | 0 | 0 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | -5.7 | 0.0 | 27 | 58 | 0 | 1 | 1 |
| 187 | 215 | 171 | 33 | 33 | 33 | 4 | 4 | 4 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 0.2 | 0.0 | 0 | 16 | 0 | 1 | 1 |
| 188 | 354 | 131 | 31 | 31 | 31 | 3 | 3 | 3 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0 | 1 | 1 |
| 189 | 362 | 34 | 33 | 33 | 33 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 2.6 | 4.7 | 0 | 0 | 0 | 1 | 1 |
| 190 | 261 | 108 | 38 | 38 | 38 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 0.0 | 0.0 | 0.0 | 1.5 | 0.0 | 0 | 23 | 0 | 1 | 1 |
| 191 | 225 | 88 | 32 | 32 | 32 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 1.6 | 0.0 | 0 | 0 | 0 | 1 | 1 |
| 192 | 279 | 98 | 32 | 32 | 32 | 2 | 2 | 2 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 1.2 | 0.0 | 0 | 0 | 0 | 1 | 1 |
| 193 | 347 | 143 | 32 | 32 | 32 | 2 | 2 | 2 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 1.1 | 0.0 | 0 | 0 | 0 | 1 | 1 |
| 194 | 317 | 68 | 36 | 36 | 36 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | -1.9 | 6.8 | 25 | 34 | 0 | 1 | 1 |
| 195 | 327 | 62 | 37 | 37 | 37 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 5.4 | 3.4 | 25 | 34 | 0 | 1 | 1 |
| 197 | 36 | 36 | 33 | 33 | 33 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 3.8 | 0.0 | 0 | 0 | 0 | 1 | 1 |
| 198 | 51 | 32 | 32 | 32 | 32 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0 | 1 | 1 |
| 199 | 350 | 217 | 34 | 34 | 34 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 0.5 | 0.0 | 0 | 0 | 0 | 1 | 1 |
| 200 | 350 | 217 | 34 | 34 | 34 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 0.5 | 0.0 | 0 | 0 | 0 | 1 | 1 |
| 201 | 27 | 107 | 37 | 37 | 37 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 1.7 | 1.3 | 0 | 23 | 0 | 1 | 1 |
| 202 | 301 | 27 | 34 | 34 | 34 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 4.7 | 0.1 | 35 | 34 | 1 | 1 | 1 |
| 203 | 304 | 34 | 33 | 33 | 33 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 1.9 | 0.7 | 25 | 34 | 0 | 1 | 1 |
| 204 | 330 | 22 | 36 | 36 | 36 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 6.7 | 1.1 | 25 | 34 | 0 | 1 | 1 |
| 205 | 337 | 61 | 36 | 36 | 36 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 1.4 | 1.1 | 21 | 34 | 0 | 1 | 1 |
| 206 | 43 | 34 | 33 | 33 | 33 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 5.8 | 0.1 | 25 | 34 | 0 | 1 | 1 |
| 207 | 34 | 34 | 33 | 33 | 33 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 1.3 | 1.7 | 22 | 56 | 2 | 4 | 1 |
| 208 | 342 | 21 | 35 | 35 | 35 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 3.0 | 1.4 | 22 | 56 | 3 | 5 | 1 |
| 209 | 34 | 34 | 33 | 33 | 33 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | -0.9 | 0.7 | 0 | 0 | 0 | 1 | 1 |
| 210 | 338 | 14 | 31 | 31 | 31 | 4 | 4 | 4 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | -3.7 | 0.6 | 0 | 0 | 0 | 2 | 1 |
| 211 | 34 | 34 | 33 | 33 | 33 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 1.0 | 1.7 | 34 | 34 | 4 | 3 | 1 |
| 212 | 34 | 34 | 33 | 33 | 33 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 4.1 | 1.1 | 25 | 34 | 0 | 1 | 1 |
| 213 | 34 | 34 | 33 | 33 | 33 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | -1.5 | 0.4 | 0 | 0 | 0 | 2 | 1 |
| 214 | 242 | 24 | 32 | 32 | 32 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 1.2 | 1.3 | 22 | 56 | 0 | 3 | 1 |
| 215 | 323 | 69 | 33 | 33 | 33 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | -0.3 | 0.2 | 25 | 34 | 1 | 1 | 1 |
| 216 | 17 | 26 | 34 | 34 | 34 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | -2.5 | 1.7 | 16 | 63 | 2 | 2 | 1 |
| 217 | 354 | 25 | 41 | 41 | 41 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 0.9 | 0.0 | 29 | 0 | 0 | 1 | 1 |
| 218 | 279 | 61 | 31 | 31 | 31 | 4 | 4 | 4 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 3.5 | 0.0 | 0 | 0 | 0 | 1 | 1 |
| 219 | 359 | 47 | 44 | 44 | 44 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 3.5 | 1.2 | 25 | 34 | 3 | 3 | 1 |
| 220 | 342 | 44 | 46 | 46 | 46 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 4.6 | 1.1 | 25 | 34 | 2 | 2 | 1 |
| 221 | 345 | 40 | 41 | 41 | 41 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 0.9 | 1.8 | 0 | 34 | 2 | 2 | 1 |
| 222 | 150 | 24 | 31 | 31 | 31 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 11.4 | 0.0 | 0 | 0 | 0 | 1 | 1 |
| 223 | 195 | 25 | 31 | 31 | 31 | 1 | 1 | 1 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | -3.1 | 0.0 | 0 | 0 | 0 | 1 | 1 |
| 224 | 345 | 67 | 45 | 47 | 47 | 5 | 5 | 5 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 3.3 | 0.9 | 22 | 56 | 2 | 2 | 1 |
| 225 | 338 | 50 | 47 | 48 | 48 | 3 | 4 | 4 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 3.3 | 0.0 | 25 | 34 | 0 | 2 | 1 |
| 226 | 136 | 30 | 35 | 35 | 35 | 2 | 2 | 2 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 8.9 | 0.0 | 0 | 0 | 0 | 1 | 1 |
| 227 | 342 | 50 | 31 | 31 | 31 | 5 | 5 | 5 | 11.8 | 2.1 | 0.00 | 1.1 | 1.1 | 0.0 | 6.2 | 0.0 | 12 | 56 | 0 | 1 | 1 |

Table A2. ACDT Volume Scan Output for Volume Scan No. 2, Case Study No. 2 (Cont'd)

| CLUSTER OUTPUT | | | | | | | | | | | | | | | | | | | |
|----------------|------|-------|-------|------|-------|-----|-----|-----|----------|------|-----|-----|-----|------|-----|-----|-----|-----|-----|
| CENTROID | | | | | | | | | | | | | | | | | | | |
| TRK | AV | PK | AV | PK | V | F | AV | PK | AV | PK | AV | PK | AV | PK | AV | PK | AV | PK | AV |
| NO | DES | KM | DES | KM | DES | KM | DES | KM | DES | KM | DES | KM | DES | KM | DES | KM | DES | KM | DES |
| 3 | 290 | 59 | 290 | 59 | 1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 4 | 301 | 82 | 301 | 82 | 1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 25 | 320 | 61 | 320 | 61 | 25 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 26 | 312 | 55 | 312 | 55 | 1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 8 | 332 | 51 | 332 | 51 | 1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 11 | 334 | 65 | 334 | 65 | 1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 27 | 1 | 64 | 35 | 17 | 3 | 1.0 | 0.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 16 | 15 | 68 | 39 | 45 | 10 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 12 | 345 | 60 | 45 | 50 | 4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 28 | 232 | 38 | 48 | 47 | 1 | 1.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 20 | 340 | 77 | 38 | 44 | 2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 22 | 346 | 72 | 40 | 47 | 5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 29 | 353 | 64 | 41 | 40 | 2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 32 | 272 | 95 | 33 | 35 | 2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 31 | 231 | 76 | 33 | 35 | 2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 32 | 340 | 56 | 36 | 43 | 2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 33 | 354 | 61 | 44 | 43 | 3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 34 | 52 | 102 | 31 | 32 | 1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 35 | 326 | 66 | 33 | 35 | 2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | | | | | | | | | | | | | | | | | | |
| VOL | H-MM | AREA | WFLX | NEAR | NEIGH | ACT | PC | NO | VELOCITY | TRK | CLS | CNT | C | OVER | | | | | |
| SCAN | KM2 | SMT/H | CELL | CLST | CNT | VOL | CS | PC | EM/S | MM/S | NC | CTR | CTF | C | | | | | |
| 2 | 1539 | 4.5 | 27.56 | 3.5 | 16.0 | 0.0 | 147 | 25 | 12 | 13.5 | 3.9 | 229 | 35 | 67 | C | C | C | C | C |

Table A3. ACDT Volume Scan Output for Volume Scan No. 3, Case Study No. 2

| | | | | | | | | | | | | | | | | | | | | |
|--|-----|-----|-----|-----|----|----|----|---|---|-----|------|-----|------|------|-----|------|------|----|----|----|
| SCAN TIME 100 154708 - 155150 WGL SCAN 3 A2 - 22.9 TC 18.5 (DEG) | | | | | | | | | | | | | | | | | | | | |
| TRACK REF TIME 154523 - 154703 AZM SCAN 9/C EL - 0.9 TC 6.5 (DEG) | | | | | | | | | | | | | | | | | | | | |
| FIXED CONTROL OUTPUT | | | | | | | | | | | | | | | | | | | | |
| CENTROID AV CELL 2 A X A SPR SER 0 WTS AREA VELOCITY NEAR MX MR SF | | | | | | | | | | | | | | | | | | | | |
| TRK | AZM | RNG | AZM | RNG | AV | FX | V | S | C | X | L | P | FLCP | XSCN | AV | CELL | DIST | HT | IC | IC |
| NO | DEG | KM | DEG | KM | DE | DE | C | C | L | KM | KM | T | MT/F | KKM2 | CFG | M/S | KM | KM | AC | AC |
| 62 | 31 | 109 | 32 | 106 | 37 | 40 | 2 | 0 | 0 | 0.0 | 0.0 | 0 | 0.44 | 0.10 | 257 | 16 | 0.0 | 2 | 0 | 0 |
| 63 | 31 | 77 | 31 | 72 | 31 | 72 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.02 | 0.01 | 559 | 999 | 0.0 | 5 | 0 | 0 |
| 69 | 37 | 56 | 37 | 56 | 33 | 33 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.01 | 0.00 | 559 | 999 | 0.0 | 0 | 0 | 0 |
| 70 | 42 | 58 | 44 | 41 | 34 | 32 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.04 | 0.01 | 559 | 999 | 0.0 | 5 | 0 | 0 |
| 71 | 50 | 130 | 50 | 131 | 33 | 35 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.03 | 0.01 | 559 | 999 | 0.0 | 6 | 0 | 0 |
| 67 | 56 | 141 | 57 | 140 | 39 | 44 | 2 | 0 | 0 | 0.0 | 0.0 | 0 | 0.72 | 0.11 | 258 | 16 | 0.0 | 6 | 0 | 0 |
| 72 | 56 | 130 | 57 | 130 | 32 | 33 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.06 | 0.02 | 559 | 999 | 0.0 | 3 | 0 | 0 |
| 73 | 126 | 28 | 120 | 29 | 37 | 40 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.05 | 0.02 | 559 | 999 | 0.0 | 2 | 0 | 0 |
| 74 | 135 | 23 | 135 | 23 | 32 | 32 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.01 | 0.00 | 559 | 999 | 0.0 | 0 | 0 | 0 |
| 15 | 233 | 215 | 233 | 215 | 41 | 45 | 3 | 1 | 1 | 0.0 | 0.0 | 27 | 4.18 | 0.50 | 272 | 12 | 0.0 | 7 | 0 | 0 |
| 75 | 241 | 221 | 240 | 223 | 37 | 37 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.52 | 0.13 | 559 | 999 | 0.0 | 5 | 0 | 0 |
| 76 | 252 | 149 | 250 | 149 | 39 | 42 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.70 | 0.11 | 559 | 999 | 0.0 | 4 | 0 | 0 |
| 16 | 236 | 183 | 236 | 186 | 42 | 47 | 5 | 1 | 1 | 1.3 | 7.3 | 56 | 5.61 | 0.64 | 241 | 6 | 4.7 | 6 | 0 | 0 |
| 77 | 258 | 123 | 257 | 120 | 34 | 35 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.12 | 0.04 | 559 | 999 | 0.0 | 3 | 0 | 0 |
| 78 | 258 | 54 | 261 | 53 | 32 | 33 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.01 | 0.00 | 559 | 999 | 0.0 | 3 | 0 | 0 |
| 43 | 259 | 110 | 260 | 109 | 35 | 37 | 1 | 1 | 1 | 0.0 | 0.0 | 0 | 0.09 | 0.02 | 277 | 13 | 0.0 | 2 | 0 | 0 |
| 79 | 264 | 75 | 264 | 74 | 32 | 32 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.01 | 0.00 | 559 | 999 | 0.0 | 1 | 0 | 0 |
| 80 | 268 | 16 | 268 | 16 | 31 | 31 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.00 | 0.00 | 559 | 999 | 0.0 | 0 | 0 | 0 |
| 81 | 285 | 69 | 286 | 67 | 35 | 38 | 1 | 1 | 1 | 0.0 | 0.0 | 0 | 0.18 | 0.05 | 559 | 999 | 0.0 | 3 | 0 | 0 |
| 82 | 270 | 83 | 270 | 82 | 33 | 35 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.01 | 0.00 | 559 | 999 | 0.0 | 4 | 0 | 0 |
| 53 | 290 | 78 | 282 | 78 | 31 | 32 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.01 | 0.00 | 189 | 5 | 0.0 | 4 | 0 | 0 |
| 23 | 270 | 97 | 272 | 97 | 34 | 44 | 4 | 1 | 1 | 3.2 | 8.7 | 23 | 0.88 | 0.19 | 226 | 15 | 0.0 | 5 | 0 | 0 |
| 83 | 282 | 65 | 284 | 64 | 33 | 34 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.03 | 0.01 | 220 | 15 | 0.0 | 4 | 0 | 0 |
| 84 | 294 | 73 | 294 | 72 | 32 | 33 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.13 | 0.04 | 215 | 13 | 0.0 | 1 | 0 | 3 |
| 85 | 296 | 67 | 296 | 67 | 31 | 31 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.01 | 0.00 | 559 | 999 | 0.0 | 0 | 0 | 0 |
| 86 | 298 | 61 | 300 | 60 | 33 | 36 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.03 | 0.01 | 559 | 999 | 0.0 | 3 | 0 | 0 |
| 3 | 306 | 82 | 306 | 80 | 35 | 37 | 3 | 2 | 2 | 4.5 | 4.9 | 42 | 0.47 | 0.14 | 254 | 16 | 0.0 | 2 | 0 | 0 |
| 87 | 331 | 34 | 331 | 34 | 32 | 32 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.01 | 0.00 | 559 | 999 | 0.0 | 0 | 0 | 0 |
| 88 | 340 | 104 | 341 | 104 | 36 | 38 | 1 | 0 | 0 | 0.0 | 0.0 | 0 | 0.09 | 0.02 | 559 | 999 | 0.0 | 2 | 0 | 0 |
| 89 | 343 | 87 | 344 | 84 | 31 | 32 | 2 | 1 | 1 | 0.0 | 0.0 | 0 | 0.02 | 0.01 | 218 | 10 | 0.0 | 4 | 0 | 0 |
| 90 | 358 | 101 | 358 | 101 | 38 | 41 | 3 | 1 | 1 | 0.5 | 4.1 | 81 | 0.31 | 0.05 | 559 | 999 | 0.0 | 2 | 0 | 0 |
| 34 | 339 | 63 | 337 | 64 | 39 | 48 | 33 | 5 | 5 | 9.0 | 16.4 | 53 | 4.79 | 0.83 | 253 | 13 | 4.0 | 7 | 56 | 0 |
| 91 | 5 | 35 | 6 | 39 | 41 | 46 | 5 | 1 | 1 | 1.3 | 5.7 | 336 | 0.27 | 0.03 | 559 | 999 | 5.1 | 5 | 0 | 0 |
| 63 | 14 | 78 | 17 | 79 | 39 | 45 | 8 | 2 | 2 | 4.5 | 5.9 | 121 | 1.47 | 0.24 | 235 | 14 | 5.1 | 8 | 0 | 0 |

Table A3. ACFT Volume Scan Output for Volume Scan No. 3, Cast Study No. 2
(Cont'd)

| VOLUME CELL OUTPUT | | | | | | | | | | | | | | | | | | | |
|--------------------|------|-----|-----|-----|-----|-----|----|----|------|------|----|------|----|-------|-----|-------|-----|----|----|
| IDENT | IC | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 |
| LINE | ACFT | RM | AV | PA | LA | MI | LS | EN | EN/2 | RM/2 | SP | SP/2 | A | (TAN) | CCF | FAC | PAC | CS | CN |
| | | MM | MM | MM | MM | MM | MM | MM | MM | MM | MM | MM | MM | (M/S) | SEC | VEL | SPS | TR | TR |
| | | | | | | | | | | | | | | (M/S) | | | | | |
| 130 | 130 | 129 | 42 | 42 | 42 | 42 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | -5.3 | 0.0 | 0 | 62 |
| 131 | 131 | 74 | 74 | 74 | 74 | 74 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0.4 | 2.1 | 0 | 68 |
| 132 | 132 | 54 | 54 | 54 | 54 | 54 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 4.2 | 0.0 | 0 | 69 |
| 133 | 133 | 44 | 44 | 44 | 44 | 44 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 3.1 | 1.6 | 0 | 70 |
| 134 | 134 | 121 | 121 | 121 | 121 | 121 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1.5 | 0.7 | 0 | 71 |
| 135 | 135 | 141 | 141 | 141 | 141 | 141 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 3.7 | 1.9 | 0 | 67 |
| 136 | 136 | 122 | 122 | 122 | 122 | 122 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0.3 | 1.2 | 0 | 72 |
| 137 | 137 | 101 | 101 | 101 | 101 | 101 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | -2.5 | 6.2 | 0 | 73 |
| 138 | 138 | 135 | 135 | 135 | 135 | 135 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | -11.1 | 0.0 | 0 | 74 |
| 139 | 139 | 141 | 141 | 141 | 141 | 141 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | -3.0 | 2.3 | 36 | 16 |
| 140 | 140 | 142 | 142 | 142 | 142 | 142 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0.0 | 0.0 | 0 | 75 |
| 141 | 141 | 143 | 143 | 143 | 143 | 143 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1.7 | 0.7 | 0 | 76 |
| 142 | 142 | 144 | 144 | 144 | 144 | 144 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | -4.0 | 4.0 | 0 | 77 |
| 143 | 143 | 145 | 145 | 145 | 145 | 145 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 4.1 | 3.1 | 0 | 78 |
| 144 | 144 | 146 | 146 | 146 | 146 | 146 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 6.0 | 2.5 | 0 | 79 |
| 145 | 145 | 147 | 147 | 147 | 147 | 147 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 2.1 | 2.1 | 0 | 80 |
| 146 | 146 | 148 | 148 | 148 | 148 | 148 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | -11.1 | 0.0 | 0 | 81 |
| 147 | 147 | 149 | 149 | 149 | 149 | 149 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | -0.1 | 2.7 | 37 | 91 |
| 148 | 148 | 150 | 150 | 150 | 150 | 150 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0.0 | 0.0 | 0 | 85 |
| 149 | 149 | 151 | 151 | 151 | 151 | 151 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1.0 | 0.1 | 38 | 15 |
| 150 | 150 | 152 | 152 | 152 | 152 | 152 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | -6.8 | 1.4 | 39 | 86 |
| 151 | 151 | 153 | 153 | 153 | 153 | 153 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1.4 | 0.0 | 0 | 16 |
| 152 | 152 | 154 | 154 | 154 | 154 | 154 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 3.1 | 3.1 | 0 | 16 |
| 153 | 153 | 155 | 155 | 155 | 155 | 155 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | -0.3 | 6.1 | 0 | 34 |
| 154 | 154 | 156 | 156 | 156 | 156 | 156 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 6.0 | 0.0 | 0 | 57 |
| 155 | 155 | 157 | 157 | 157 | 157 | 157 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | -3.8 | 0.3 | 0 | 58 |
| 156 | 156 | 158 | 158 | 158 | 158 | 158 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | -0.1 | 3.3 | 28 | 99 |
| 157 | 157 | 159 | 159 | 159 | 159 | 159 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | -4.4 | 0.0 | 0 | 90 |
| 158 | 158 | 160 | 160 | 160 | 160 | 160 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | -5.8 | 4.7 | 40 | 90 |
| 159 | 159 | 161 | 161 | 161 | 161 | 161 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | -1.0 | 5.0 | 41 | 23 |
| 160 | 160 | 162 | 162 | 162 | 162 | 162 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 3.1 | 3.0 | 42 | 51 |
| 161 | 161 | 163 | 163 | 163 | 163 | 163 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | -4.6 | 1.3 | 1 | 94 |
| 162 | 162 | 164 | 164 | 164 | 164 | 164 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | -5.0 | 1.1 | 4 | 2 |
| 163 | 163 | 165 | 165 | 165 | 165 | 165 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | -7.0 | 1.1 | 39 | 34 |
| 164 | 164 | 166 | 166 | 166 | 166 | 166 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0.7 | 1.3 | 33 | 15 |
| 165 | 165 | 167 | 167 | 167 | 167 | 167 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0.7 | 0.7 | 1 | 16 |
| 166 | 166 | 168 | 168 | 168 | 168 | 168 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0.0 | 0.0 | 0 | 0 |
| 167 | 167 | 169 | 169 | 169 | 169 | 169 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0.0 | 0.0 | 0 | 0 |
| 168 | 168 | 170 | 170 | 170 | 170 | 170 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | -0.9 | 6.0 | 39 | 34 |
| 169 | 169 | 171 | 171 | 171 | 171 | 171 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | -7.1 | 1.0 | 47 | 50 |
| 170 | 170 | 172 | 172 | 172 | 172 | 172 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1.9 | 1.4 | 25 | 34 |
| 171 | 171 | 173 | 173 | 173 | 173 | 173 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 7.8 | 1.8 | 43 | 74 |
| 172 | 172 | 174 | 174 | 174 | 174 | 174 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | -0.7 | 1.6 | 43 | 34 |
| 173 | 173 | 175 | 175 | 175 | 175 | 175 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0.7 | 0.9 | 22 | 34 |
| 174 | 174 | 176 | 176 | 176 | 176 | 176 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 5.1 | 2.2 | 25 | 34 |
| 175 | 175 | 177 | 177 | 177 | 177 | 177 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0.0 | 0.0 | 16 | 34 |
| 176 | 176 | 178 | 178 | 178 | 178 | 178 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 4.4 | 0.0 | 1 | 74 |
| 177 | 177 | 179 | 179 | 179 | 179 | 179 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 2.0 | 1.8 | 12 | 34 |
| 178 | 178 | 180 | 180 | 180 | 180 | 180 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1.0 | 0.0 | 0 | 0 |
| 179 | 179 | 181 | 181 | 181 | 181 | 181 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | -0.7 | 0.0 | 0 | 0 |

Table A3. ACDT Volume Scan Output for Volume Scan No. 3, Case Study No. 2 (Cont'd)

| | | | | | | | | | | | | | | | | | | | | |
|-----|-----|-----|----|----|----|----|---|---|------|-----|------|------|-----|-----|-------|-----|-----|----|----|---|
| 170 | 14 | 72 | 32 | 33 | 32 | 32 | 4 | 4 | 11.3 | 3.9 | 0.00 | 7.4 | 0.0 | 0.0 | -3.0 | 1.0 | 0 | 0 | 0 | 1 |
| 171 | 150 | 71 | 35 | 26 | 31 | 20 | 3 | 7 | 11.3 | 3.9 | 0.00 | 4.1 | 1.0 | 0.0 | -1.0 | 0.0 | 0 | 0 | 0 | 1 |
| 172 | 334 | 51 | 36 | 18 | 31 | 11 | 1 | 1 | 11.3 | 3.9 | 0.00 | 4.1 | 1.0 | 0.0 | -0.7 | 1.4 | 16 | 0 | 2 | 4 |
| 173 | 334 | 51 | 40 | 46 | 40 | 44 | 2 | 7 | 11.3 | 3.9 | 0.00 | 0.3 | 1.0 | 0.0 | -0.5 | 1.0 | 18 | 34 | 0 | 0 |
| 174 | 17 | 32 | 41 | 40 | 40 | 41 | 1 | 1 | 11.3 | 3.9 | 0.00 | 1.1 | 1.0 | 0.0 | -0.7 | 0.0 | 40 | 91 | 1 | 3 |
| 175 | 324 | 74 | 33 | 35 | 31 | 25 | 7 | 1 | 11.3 | 3.9 | 0.00 | 0.3 | 1.0 | 0.0 | -1.0 | 3.8 | 39 | 34 | 1 | 2 |
| 180 | 17 | 70 | 34 | 34 | 34 | 34 | 4 | 4 | 11.3 | 3.9 | 0.00 | 0.3 | 1.0 | 0.0 | -0.7 | 0.0 | 16 | 0 | 0 | 0 |
| 176 | 243 | 93 | 30 | 30 | 32 | 30 | 3 | 3 | 11.3 | 3.9 | 0.00 | 0.1 | 1.0 | 0.0 | -0.3 | 0.0 | 0 | 0 | 0 | 1 |
| 177 | 1 | 47 | 73 | 37 | 33 | 33 | 3 | 3 | 11.3 | 3.9 | 0.00 | 0.1 | 1.0 | 0.0 | -0.0 | 1.7 | 0 | 0 | 1 | 1 |
| 178 | 121 | 41 | 27 | 27 | 25 | 25 | 1 | 1 | 11.3 | 3.9 | 0.00 | 0.1 | 1.0 | 0.0 | -0.5 | 0.1 | 16 | 0 | 1 | 1 |
| 179 | 47 | 65 | 34 | 34 | 34 | 34 | 3 | 3 | 11.3 | 3.9 | 0.00 | 0.1 | 1.0 | 0.0 | -1.0 | 0.0 | 0 | 0 | 0 | 1 |
| 183 | 351 | 34 | 29 | 29 | 28 | 28 | 3 | 3 | 11.3 | 3.9 | 0.00 | 0.1 | 1.0 | 0.0 | -0.1 | 0.0 | 16 | 34 | 1 | 0 |
| 180 | 265 | 50 | 32 | 30 | 32 | 32 | 3 | 3 | 11.3 | 3.9 | 0.00 | 0.1 | 1.0 | 0.0 | -0.1 | 1.0 | 0 | 0 | 0 | 1 |
| 181 | 446 | 4 | 24 | 23 | 24 | 24 | 3 | 3 | 11.3 | 3.9 | 0.00 | 0.1 | 1.0 | 0.0 | -5.0 | 1.1 | 0 | 0 | 0 | 1 |
| 181 | 305 | 76 | 31 | 31 | 31 | 31 | 1 | 1 | 11.3 | 3.9 | 0.00 | 1.0 | 0.0 | 0.0 | -0.0 | 0.0 | 0 | 0 | 0 | 1 |
| 182 | 12 | 41 | 41 | 42 | 42 | 41 | 1 | 1 | 11.3 | 3.9 | 0.00 | 0.0 | 1.0 | 0.0 | -1.0 | 0.0 | 40 | 91 | 0 | 1 |
| 183 | 310 | 41 | 31 | 31 | 31 | 31 | 3 | 3 | 11.3 | 3.9 | 0.00 | 1.0 | 0.0 | 0.0 | -0.0 | 0.0 | 0 | 0 | 0 | 1 |
| 183 | 346 | 40 | 3 | 3 | 3 | 3 | 3 | 3 | 11.3 | 3.9 | 0.00 | 0.1 | 1.0 | 0.0 | -0.0 | 0.0 | 0 | 0 | 0 | 1 |
| 184 | 340 | 67 | 31 | 31 | 31 | 31 | 3 | 3 | 11.3 | 3.9 | 0.00 | 0.1 | 1.0 | 0.0 | -0.0 | 0.0 | 0 | 0 | 0 | 1 |
| 181 | 210 | 61 | 31 | 32 | 31 | 31 | 1 | 1 | 11.3 | 3.9 | 0.00 | 0.1 | 1.0 | 0.0 | -0.5 | 0.3 | 39 | 35 | 0 | 0 |
| 189 | 315 | 57 | 41 | 41 | 41 | 41 | 1 | 1 | 11.3 | 3.9 | 0.00 | 0.0 | 1.0 | 0.0 | -0.0 | 0.0 | 1.3 | 39 | 34 | 1 |
| 189 | 250 | 79 | 37 | 39 | 37 | 37 | 1 | 1 | 11.3 | 3.9 | 0.00 | 0.7 | 1.0 | 0.0 | -0.5 | 4.1 | 22 | 34 | 6 | 3 |
| 188 | 17 | 64 | 40 | 43 | 40 | 43 | 1 | 1 | 11.3 | 3.9 | 0.00 | 1.0 | 0.0 | 0.0 | -11.7 | 0.0 | 16 | 63 | 1 | 0 |
| 182 | 240 | 82 | 34 | 35 | 35 | 34 | 2 | 3 | 11.3 | 3.9 | 0.00 | 0.0 | 1.0 | 0.0 | -1.0 | 1.0 | 0 | 23 | 2 | 2 |
| 186 | 350 | 72 | 45 | 46 | 46 | 46 | 1 | 1 | 11.3 | 3.9 | 0.00 | 0.7 | 1.0 | 0.0 | -0.0 | 0.0 | 7.5 | 28 | 34 | 0 |
| 182 | 349 | 56 | 41 | 45 | 42 | 45 | 3 | 5 | 11.3 | 3.9 | 0.00 | 1.0 | 0.0 | 0.0 | -2.0 | 2.0 | 12 | 34 | 2 | 2 |
| 183 | 357 | 57 | 36 | 36 | 36 | 36 | 4 | 4 | 11.3 | 3.9 | 0.00 | 0.3 | 1.0 | 0.0 | -0.3 | 0.0 | 12 | 34 | 1 | 0 |
| 189 | 11 | 59 | 38 | 38 | 38 | 38 | 1 | 1 | 11.3 | 3.9 | 0.00 | 0.5 | 2.0 | 0.0 | -3.0 | 4.9 | 0 | 63 | 4 | 0 |
| 181 | 15 | 79 | 35 | 38 | 38 | 37 | 1 | 1 | 11.3 | 3.9 | 0.00 | 0.1 | 0.0 | 0.0 | -7.7 | 0.0 | 44 | 63 | 0 | 2 |
| 181 | 347 | 81 | 40 | 41 | 40 | 41 | 1 | 1 | 11.3 | 3.9 | 0.00 | 0.7 | 3.1 | 0.0 | -3.0 | 5.9 | 63 | 34 | 9 | 3 |
| 181 | 16 | 83 | 41 | 40 | 40 | 40 | 1 | 1 | 11.3 | 3.9 | 0.00 | 11.0 | 3.9 | 0.0 | -4.7 | 5.0 | 44 | 63 | 1 | 1 |
| 182 | 16 | 76 | 37 | 37 | 37 | 37 | 1 | 1 | 11.3 | 3.9 | 0.00 | 2.0 | 3.3 | 0.0 | -0.0 | 0.0 | 0 | 63 | 1 | 0 |
| 147 | 20 | 77 | 42 | 45 | 37 | 37 | 1 | 1 | 11.3 | 3.9 | 0.00 | 3.0 | 1.7 | 0.0 | -0.0 | 1.7 | 16 | 63 | 5 | 3 |
| 180 | 136 | 176 | 33 | 33 | 32 | 32 | 5 | 5 | 11.3 | 3.9 | 0.00 | 12.1 | 0.0 | 0.0 | -0.2 | 0.0 | 76 | 16 | 0 | 1 |
| 189 | 260 | 109 | 35 | 37 | 37 | 37 | 1 | 0 | 11.3 | 3.9 | 0.00 | 4.0 | 1.1 | 0.0 | 3.7 | 2.1 | 45 | 43 | 1 | 2 |
| 184 | 232 | 73 | 31 | 32 | 31 | 31 | 1 | 0 | 11.3 | 3.9 | 0.00 | 2.3 | 0.0 | 0.0 | -0.3 | 0.4 | 0 | 53 | 0 | 4 |
| 185 | 232 | 71 | 33 | 34 | 34 | 32 | 1 | 3 | 11.3 | 3.9 | 0.00 | 3.4 | 0.0 | 0.0 | -2.2 | 0.3 | 0 | 0 | 0 | 2 |
| 188 | 311 | 35 | 35 | 37 | 37 | 32 | 1 | 1 | 11.3 | 3.9 | 0.00 | 4.4 | 2.2 | 0.0 | -3.1 | 2.8 | 0 | 3 | 1 | 2 |
| 178 | 35 | 104 | 33 | 34 | 34 | 33 | 1 | 2 | 11.3 | 3.9 | 0.00 | 10.2 | 1.3 | 0.0 | -1.7 | 4.4 | 0 | 62 | 2 | 2 |
| 183 | 59 | 116 | 34 | 37 | 37 | 31 | 2 | 3 | 11.3 | 3.9 | 0.00 | 4.6 | 1.0 | 0.0 | -0.8 | 3.0 | 0 | 67 | 1 | 2 |
| 184 | 303 | 75 | 34 | 34 | 34 | 34 | 1 | 1 | 11.3 | 3.9 | 0.00 | 3.3 | 1.3 | 0.0 | -5.0 | 0.2 | 46 | 3 | 1 | 1 |
| 192 | 240 | 94 | 32 | 32 | 32 | 32 | 1 | 1 | 11.3 | 3.9 | 0.00 | 1.0 | 0.0 | 0.0 | -1.0 | 0.0 | 0 | 23 | 0 | 1 |
| 194 | 319 | 66 | 34 | 35 | 35 | 35 | 2 | 3 | 11.3 | 3.9 | 0.00 | 4.2 | 4.5 | 0.0 | -7.7 | 2.3 | 39 | 34 | 2 | 3 |
| 129 | 232 | 268 | 40 | 40 | 40 | 40 | 5 | 5 | 11.3 | 3.9 | 0.00 | 9.4 | 0.0 | 0.0 | -1.0 | 0.0 | 0 | 15 | 0 | 1 |
| 201 | 273 | 102 | 36 | 36 | 36 | 36 | 1 | 1 | 11.3 | 3.9 | 0.00 | 4.9 | 0.0 | 0.0 | -2.9 | 0.0 | 41 | 23 | 0 | 1 |
| 202 | 329 | 87 | 32 | 32 | 32 | 32 | 2 | 2 | 11.3 | 3.9 | 0.00 | 1.0 | 2.7 | 0.0 | -2.3 | 0.2 | 35 | 34 | 2 | 0 |
| 203 | 335 | 75 | 34 | 37 | 37 | 32 | 1 | 3 | 11.3 | 3.9 | 0.00 | 6.0 | 1.4 | 0.0 | -6.3 | 2.8 | 25 | 34 | 3 | 2 |
| 204 | 316 | 62 | 37 | 37 | 37 | 37 | 0 | 0 | 11.3 | 3.9 | 0.00 | 3.5 | 4.1 | 0.0 | -11.7 | 0.0 | 0 | 34 | 1 | 0 |
| 205 | 342 | 69 | 41 | 43 | 43 | 41 | 0 | 3 | 11.3 | 3.9 | 0.00 | 3.1 | 1.3 | 0.0 | -6.0 | 4.1 | 12 | 34 | 2 | 3 |
| 206 | 344 | 82 | 31 | 31 | 31 | 31 | 4 | 4 | 11.3 | 3.9 | 0.00 | 2.3 | 0.0 | 0.0 | -3.0 | 0.0 | 28 | 89 | 0 | 1 |

Table A3. ACDT Volume Scan Output for Volume Scan No. 3, Case Study No. 2 (Cont'd)

| | | | | | | | | | | | | | | | | | | | | | | |
|------|-----|----|----|----|----|----|---|---|---|------|------|------|-----|-----|-----|------|-----|----|----|---|---|---|
| 207 | 342 | 80 | 33 | 33 | 33 | 33 | 1 | 1 | 1 | 10.0 | 6.0 | 0.00 | 3.0 | 1.2 | C.C | -6.6 | 0.0 | 22 | 34 | 1 | 1 | 2 |
| 208 | 352 | 71 | 40 | 40 | 40 | 40 | 1 | 1 | 1 | 12.1 | 3.4 | 0.00 | 1.8 | 4.0 | C.C | -8.2 | 5.3 | 22 | 34 | 2 | C | 2 |
| 209 | 26 | 71 | 36 | 36 | 36 | 36 | 3 | 3 | 3 | 10.3 | 6.4 | 0.00 | 1.6 | C.C | C.C | -2.6 | 0.0 | 0 | C | 0 | 1 | 2 |
| 211 | 329 | 84 | 36 | 40 | 34 | 33 | 2 | 4 | 6 | 13.5 | 2.6 | 1.42 | 6.1 | 2.2 | C.C | 3.3 | 5.1 | 35 | 34 | 3 | 3 | 2 |
| 213 | 16 | 86 | 35 | 35 | 35 | 35 | 3 | 4 | 4 | 8.3 | 6.4 | 0.00 | 4.2 | 1.4 | C.C | -1.9 | 0.8 | 44 | 63 | 4 | 2 | 2 |
| 214 | 353 | 72 | 36 | 36 | 36 | 36 | 1 | 1 | 1 | 14.7 | -1.0 | 0.00 | 5.2 | 1.5 | C.C | 4.8 | 0.0 | 22 | 34 | 1 | 0 | 2 |
| 215 | 308 | 65 | 31 | 32 | 31 | 32 | 1 | 2 | 2 | 14.9 | 4.3 | 0.00 | 4.6 | 1.7 | C.C | -7.3 | 0.7 | 39 | 34 | 1 | 2 | 2 |
| 216 | 22 | 81 | 37 | 38 | 37 | 38 | 1 | 3 | 4 | 16.7 | 4.7 | 0.00 | 4.1 | 1.8 | C.C | -3.9 | 3.3 | 16 | 63 | 5 | 3 | 2 |
| 218 | 284 | 64 | 33 | 34 | 34 | 31 | C | 2 | 4 | 10.6 | 7.9 | 2.42 | 4.1 | 1.0 | C.C | 2.1 | 1.4 | 37 | 83 | C | 5 | 1 |
| 219* | 350 | 51 | 46 | 42 | 45 | 46 | C | 2 | 4 | 16.3 | 12.2 | 3.90 | 3.4 | 1.3 | C.C | 0.5 | 1.4 | 12 | 34 | 6 | 5 | 1 |
| 224 | 347 | 66 | 38 | 40 | 40 | 35 | C | 2 | 5 | 8.5 | 0.3 | 4.32 | 3.9 | 1.4 | C.C | 4.7 | 3.4 | 22 | 34 | 6 | 6 | 1 |
| 227* | 346 | 59 | 41 | 44 | 44 | 39 | 2 | 3 | 5 | 10.6 | 4.2 | 3.73 | 3.2 | 1.2 | C.C | 1.9 | 1.1 | 12 | 34 | 1 | 4 | 1 |

| CLUSTER OUTPUT | | | | | | | | | | | | | | | | | | | | | | |
|----------------|-----|-----|----|----|---|-----|------|-----|----|------|------|------|----|----|----|-------|------|----|--|--|--|--|
| TRK | AZM | RNG | AV | PK | V | X | L | ANG | IC | AV | CELL | MSKM | HT | IC | IC | RECT | DIV | RT | | | | |
| NO | DEG | M | DB | DE | C | MM | KM | DEG | | EM/S | NM/S | | KM | AC | NC | MSKM | MSKM | CS | | | | |
| 36 | 236 | 178 | 38 | 41 | 2 | 0.0 | 0.0 | C | 16 | 1.5 | 3.7 | 1.0 | 5 | C | C | C.00 | 0.00 | 0 | | | | |
| 37 | 285 | 65 | 34 | 38 | 2 | 0.0 | 0.0 | C | 81 | 9.8 | 11.7 | 1.0 | 4 | C | C | C.00 | 0.00 | C | | | | |
| 38 | 233 | 219 | 42 | 45 | 2 | 0.0 | 0.0 | C | 15 | 14.4 | 6.6 | C.C | 7 | C | C | C.00 | 0.00 | C | | | | |
| 39 | 314 | 64 | 35 | 40 | 8 | 1.7 | 10.1 | 15 | 34 | 7.7 | 2.7 | 2.8 | 4 | C | 25 | -2.01 | 3.67 | 6 | | | | |
| 28 | 344 | 84 | 31 | 32 | 2 | 0.0 | 0.0 | C | 89 | 6.4 | 8.2 | C.6 | 4 | C | C | C.00 | 0.00 | 0 | | | | |
| 40 | 359 | 102 | 39 | 41 | 2 | 0.0 | 0.0 | C | 90 | 0.0 | C.C | 1.7 | 2 | C | C | C.00 | 0.00 | C | | | | |
| 41 | 271 | 99 | 38 | 44 | 2 | 0.0 | 0.0 | C | 23 | 13.4 | 13.7 | C.9 | 5 | C | C | C.00 | 0.00 | C | | | | |
| 42 | 7 | 39 | 43 | 46 | 3 | 1.9 | 1.9 | 44 | 91 | 0.0 | C.C | 1.1 | 4 | C | C | C.00 | 0.00 | C | | | | |
| 4 | 303 | 82 | 37 | 37 | 1 | 0.0 | 0.0 | C | 3 | 13.1 | 13.0 | 1.2 | 1 | C | C | C.00 | 0.00 | C | | | | |
| 25 | 338 | 69 | 36 | 41 | 4 | 1.9 | 4.4 | 309 | 34 | 14.1 | 9.3 | 1.9 | 4 | 11 | C | -0.86 | 4.53 | 3 | | | | |
| 43 | 329 | 74 | 37 | 41 | 2 | 1.1 | 5.3 | 316 | 34 | 16.4 | 5.1 | 2.9 | 3 | C | 25 | -0.24 | 4.69 | 3 | | | | |
| 22 | 351 | 72 | 39 | 46 | 8 | 3.1 | 4.3 | 322 | 34 | 16.1 | 3.0 | 1.8 | 7 | C | C | -1.13 | 4.58 | 6 | | | | |
| 12 | 342 | 55 | 43 | 48 | 8 | 2.1 | 4.7 | 308 | 34 | 13.7 | 3.6 | 1.4 | 6 | 25 | C | -1.12 | 4.15 | 6 | | | | |
| 16 | 19 | 76 | 39 | 45 | 6 | 1.2 | 5.9 | 39 | 63 | 15.2 | 7.6 | 2.3 | 8 | C | C | 1.04 | 4.51 | 4 | | | | |
| 44 | 16 | 83 | 38 | 40 | 3 | 0.0 | 2.7 | 30 | 63 | 9.5 | 6.9 | 3.2 | 4 | C | 16 | 3.17 | 4.88 | 3 | | | | |
| 45 | 260 | 109 | 35 | 37 | 1 | 0.0 | 0.0 | C | 43 | 13.4 | -1.5 | 1.1 | 2 | C | C | C.00 | 0.00 | C | | | | |
| 46 | 303 | 75 | 34 | 34 | 1 | 0.0 | 0.0 | C | 3 | 14.3 | -3.5 | 1.3 | 1 | C | 4 | C.00 | 0.00 | 0 | | | | |
| 35 | 329 | 86 | 35 | 40 | 2 | 0.0 | 0.0 | C | C | 12.9 | 1.9 | 2.3 | 6 | C | C | C.00 | 0.00 | C | | | | |

| VOL | HHMM | AREA | WFLUX | NEAR | NEIGHBOR | ACT | NC | NC | VELOCITY | TRK | CLS | CNT | G | OVER |
|------|------|------|-------|------|----------|-----|-----|----|----------|------|------|-----|-----|----------------|
| SCAN | | KMP2 | KMT/H | CELL | CLST | CNT | VCL | CS | FC | EM/S | NM/S | NC | CTR | CTR |
| 3 | 1545 | 3.5 | 21.83 | 6.0 | 19.6 | C.0 | 113 | 18 | 10 | 12.5 | 4.6 | 284 | 46 | 91 C 0 C C C 0 |

Table A4. AC/DT Volume Scan Output for Volume Scan No. 4, Case Study No. 2

| SCAN TIME 100 155022 - 155745 VOL SCAN 14.41 - 40.3 TO 39.4 (DEG) | | | | | | | | | |
|---|-----|-----|-----|-----|-----|-----|----|---|---|
| TRACK REF TIME 155115 - 155227 42" SCAN 970 EL - 0.4 TO 0.5 (DEG) | | | | | | | | | |
| FIXED CONTROL OUTPUT | | | | | | | | | |
| TRK | AZM | RNG | AZM | RNG | AV | SP | V | S | C |
| NO | DEG | KM | DEG | KM | DEG | DEG | 0 | 0 | 0 |
| 92 | 57 | 115 | 57 | 115 | 34 | 36 | 1 | 0 | 0 |
| 93 | 47 | 123 | 48 | 126 | 32 | 32 | 1 | 0 | 0 |
| 94 | 48 | 135 | 49 | 135 | 32 | 32 | 1 | 0 | 0 |
| 95 | 50 | 157 | 53 | 155 | 31 | 31 | 1 | 0 | 0 |
| 96 | 105 | 29 | 106 | 22 | 33 | 33 | 1 | 0 | 0 |
| 97 | 241 | 215 | 241 | 214 | 43 | 43 | 1 | 0 | 0 |
| 16 | 234 | 123 | 235 | 124 | 44 | 44 | 4 | 2 | 2 |
| 27 | 255 | 144 | 253 | 142 | 41 | 41 | 1 | 1 | 1 |
| 98 | 247 | 183 | 247 | 183 | 32 | 32 | 1 | 0 | 0 |
| 99 | 315 | 102 | 316 | 102 | 30 | 30 | 1 | 0 | 0 |
| 100 | 250 | 12 | 222 | 1 | 21 | 21 | 1 | 0 | 0 |
| 101 | 261 | 117 | 261 | 116 | 40 | 34 | 1 | 0 | 0 |
| 102 | 270 | 49 | 276 | 48 | 34 | 36 | 4 | 2 | 2 |
| 103 | 276 | 32 | 277 | 31 | 32 | 33 | 1 | 0 | 0 |
| 23 | 274 | 95 | 269 | 96 | 35 | 28 | 6 | 1 | 1 |
| 34 | 340 | 69 | 339 | 69 | 39 | 46 | 25 | 5 | 0 |
| 104 | 301 | 29 | 301 | 28 | 31 | 31 | 1 | 0 | 0 |
| 3 | 300 | 75 | 295 | 72 | 34 | 39 | 13 | 1 | 1 |
| 105 | 309 | 52 | 310 | 51 | 31 | 31 | 1 | 0 | 0 |
| 106 | 340 | 106 | 341 | 107 | 35 | 35 | 1 | 0 | 0 |
| 107 | 338 | 100 | 338 | 100 | 34 | 26 | 2 | 0 | 0 |
| 108 | 347 | 111 | 346 | 111 | 32 | 22 | 1 | 0 | 0 |
| 109 | 343 | 24 | 343 | 24 | 31 | 31 | 1 | 0 | 0 |
| 89 | 348 | 26 | 348 | 26 | 31 | 31 | 1 | 0 | 0 |
| 110 | 345 | 92 | 343 | 91 | 31 | 31 | 1 | 0 | 0 |
| 90 | 358 | 107 | 358 | 105 | 35 | 41 | 2 | 0 | 0 |
| 111 | 28 | 89 | 29 | 85 | 34 | 34 | 1 | 0 | 0 |
| 63 | 17 | 84 | 19 | 89 | 40 | 47 | 9 | 4 | 4 |
| 112 | 7 | 46 | 6 | 49 | 38 | 42 | 4 | 1 | 1 |
| 113 | 1 | 108 | 2 | 107 | 33 | 33 | 1 | 0 | 0 |
| 62 | 33 | 115 | 34 | 114 | 33 | 33 | 1 | 0 | 0 |
| 114 | 29 | 121 | 29 | 119 | 36 | 36 | 1 | 0 | 0 |
| 115 | 38 | 112 | 33 | 112 | 32 | 32 | 1 | 0 | 0 |
| 116 | 41 | 68 | 42 | 72 | 36 | 40 | 3 | 0 | 0 |

Table A4. ACDT Volume Scan Output for Volume Scan No. 4, Case Study No. 2 (Contd)

| VOLUME CELL OUTPUT | | | | | | | | | | | | | | | | | | | |
|--------------------|-----|-----|----|----|----|----|----|----|------|------|------|------|-----|-----|-------|-----|----|-----|----|
| TRA | AZM | RNG | AV | PK | LA | HI | LM | FM | EM | AM | SP | SP | SP | SP | SP | SP | SP | SP | SP |
| NO | DEG | KM | DB | DB | DB | DB | DB | DB | DB | DB | DB | DB | DB | DB | DB | DB | DB | DB | DB |
| 230 | 34 | 114 | 33 | 33 | 33 | 33 | 1 | 1 | 20.2 | 3.4 | 0.00 | 4.7 | 0.0 | 0.0 | -3.9 | 0.0 | 0 | 62 | 0 |
| 235 | 55 | 147 | 45 | 45 | 45 | 45 | 2 | 2 | 11.9 | 10.0 | 0.00 | 5.2 | 1.3 | 0.0 | 1.3 | 3.9 | 47 | 67 | 3 |
| 238 | 129 | 28 | 35 | 35 | 35 | 35 | 1 | 1 | 10.0 | -0.6 | 0.00 | 1.5 | 1.2 | 0.0 | 5.1 | 0.0 | 0 | 0 | 1 |
| 239 | 237 | 173 | 41 | 41 | 41 | 41 | 2 | 2 | 5.5 | 8.7 | 0.00 | 9.2 | 1.7 | 0.0 | -0.4 | 6.0 | 0 | 16 | 3 |
| 240 | 240 | 217 | 45 | 45 | 45 | 45 | 4 | 4 | 16.5 | 7.0 | 0.00 | 5.5 | 0.0 | 0.0 | 0.1 | 0.0 | 0 | 75 | 0 |
| 285 | 48 | 126 | 32 | 32 | 32 | 32 | 1 | 2 | 12.5 | 4.6 | 0.00 | 5.9 | 0.2 | 0.0 | 0.0 | 0.0 | 0 | 93 | 0 |
| 247 | 291 | 66 | 36 | 36 | 36 | 36 | 0 | 1 | 10.0 | 11.8 | 4.62 | 9.8 | 1.2 | 0.0 | -3.4 | 1.5 | 37 | 3 | 2 |
| 249 | 300 | 61 | 31 | 32 | 31 | 32 | 2 | 2 | 16.9 | 4.5 | 0.00 | 5.6 | 1.3 | 0.0 | -6.9 | 0.7 | 48 | 0 | 3 |
| 21 | 233 | 208 | 46 | 46 | 46 | 46 | 4 | 4 | 17.9 | 9.5 | 0.00 | 16.2 | 0.0 | 0.0 | 0.1 | 0.0 | 38 | 16 | 0 |
| 23 | 235 | 188 | 44 | 47 | 47 | 38 | 5 | 5 | 16.6 | 5.3 | 0.00 | 7.5 | 0.0 | 0.0 | -0.1 | 0.5 | 0 | 16 | 0 |
| 24 | 237 | 186 | 44 | 44 | 44 | 44 | 3 | 3 | 4.6 | 5.5 | 0.00 | 26.6 | 1.6 | 0.0 | 3.9 | 1.5 | 49 | 16 | 1 |
| 250 | 317 | 67 | 35 | 37 | 33 | 38 | 0 | 1 | 16.8 | 2.2 | 0.00 | 5.6 | 2.3 | 0.0 | -5.3 | 7.1 | 39 | 34 | 3 |
| 266 | 49 | 135 | 32 | 32 | 32 | 32 | 2 | 2 | 12.5 | 4.6 | 0.00 | 9.1 | 0.0 | 0.0 | 0.3 | 0.0 | 0 | 94 | 0 |
| 253 | 348 | 66 | 31 | 31 | 31 | 31 | 1 | 1 | 17.2 | 5.6 | 0.00 | 12.6 | 1.6 | 0.0 | -7.3 | 0.0 | 0 | 29 | 1 |
| 254 | 356 | 104 | 34 | 34 | 34 | 34 | 1 | 1 | 10.7 | 5.0 | 0.00 | 3.3 | 1.2 | 0.0 | -4.1 | 0.0 | 0 | 90 | 1 |
| 32 | 271 | 94 | 37 | 37 | 37 | 37 | 2 | 2 | 12.5 | 12.7 | 0.00 | 12.3 | 0.0 | 0.0 | 1.1 | 0.0 | 0 | 23 | 0 |
| 267 | 50 | 118 | 34 | 35 | 31 | 36 | 1 | 3 | 12.5 | 4.6 | 0.00 | 5.3 | 0.0 | 0.0 | 0.1 | 0.1 | 0 | 92 | 0 |
| 268 | 53 | 166 | 31 | 31 | 31 | 31 | 2 | 2 | 12.5 | 4.9 | 0.00 | 14.6 | 0.0 | 0.0 | -0.3 | 0.0 | 0 | 55 | 0 |
| 289 | 60 | 148 | 34 | 34 | 34 | 34 | 2 | 2 | 12.5 | 4.6 | 0.00 | 16.2 | 0.0 | 0.0 | 1.4 | 0.0 | 0 | 67 | 0 |
| 290 | 106 | 26 | 33 | 33 | 33 | 33 | 0 | 0 | 12.5 | 4.6 | 0.00 | 2.5 | 1.0 | 0.0 | 15.8 | 0.0 | 0 | 56 | 0 |
| 38 | 297 | 65 | 35 | 37 | 37 | 34 | 2 | 3 | 15.8 | -0.5 | 0.00 | 5.5 | 1.7 | 0.0 | -4.1 | 1.1 | 48 | 0 | 3 |
| 291 | 222 | 6 | 21 | 31 | 31 | 31 | 0 | 0 | 12.5 | 4.9 | 0.00 | 2.1 | 1.5 | 0.0 | -0.5 | 0.0 | 0 | 100 | 0 |
| 40 | 306 | 93 | 39 | 39 | 39 | 39 | 1 | 1 | 5.0 | 13.6 | 0.00 | 5.2 | 0.0 | 0.0 | -0.3 | 0.0 | 0 | 3 | 0 |
| 292 | 247 | 188 | 38 | 38 | 38 | 38 | 1 | 3 | 12.5 | 4.6 | 0.00 | 4.5 | 0.0 | 0.0 | 0.3 | 0.0 | 0 | 98 | 0 |
| 42 | 303 | 61 | 34 | 37 | 37 | 31 | 0 | 0 | 3.9 | 5.0 | 0.00 | 6.7 | 0.0 | 0.0 | -6.7 | 4.2 | 39 | 34 | 1 |
| 293 | 255 | 143 | 40 | 41 | 41 | 40 | 2 | 2 | 10.5 | 4.6 | 0.00 | 5.6 | 0.0 | 0.0 | 2.1 | 1.0 | 50 | 97 | 0 |
| 294 | 2 | 116 | 32 | 34 | 34 | 31 | 1 | 2 | 12.5 | 4.6 | 0.00 | 5.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 101 | 0 |
| 295 | 264 | 106 | 35 | 37 | 37 | 34 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.5 | 0.0 | 0.0 | 1.3 | 1.1 | 51 | 23 | 0 |
| 296 | 262 | 100 | 32 | 32 | 32 | 32 | 1 | 1 | 12.5 | 4.6 | 0.00 | 7.4 | 0.0 | 0.0 | 0.1 | 0.1 | 51 | 23 | 0 |
| 299 | 272 | 62 | 34 | 37 | 37 | 32 | 0 | 1 | 12.5 | 4.6 | 0.00 | 3.2 | 1.1 | 0.0 | 0.3 | 2.8 | 0 | 3 | 0 |
| 262 | 283 | 81 | 31 | 31 | 31 | 31 | 1 | 1 | 10.9 | 1.2 | 0.00 | 5.2 | 0.0 | 0.0 | -0.9 | 0.0 | 52 | 0 | 0 |
| 53 | 323 | 68 | 36 | 39 | 39 | 33 | 0 | 1 | 3.7 | -2.2 | 0.00 | 5.5 | 1.5 | 0.0 | -6.1 | 7.6 | 0 | 34 | 2 |
| 263 | 2 | 107 | 33 | 33 | 33 | 33 | 1 | 1 | 12.3 | 10.8 | 0.00 | 5.6 | 1.2 | 0.0 | -10.1 | 0.0 | 0 | 113 | 1 |
| 297 | 277 | 81 | 32 | 33 | 33 | 31 | 1 | 1 | 12.5 | 4.6 | 0.00 | 6.8 | 1.0 | 0.0 | -0.9 | 1.6 | 0 | 103 | 0 |
| 298 | 287 | 72 | 34 | 36 | 34 | 32 | 0 | 1 | 12.5 | 4.6 | 0.00 | 5.4 | 0.0 | 0.0 | -3.1 | 0.4 | 37 | 3 | 0 |
| 58 | 337 | 70 | 36 | 36 | 36 | 36 | 0 | 0 | 26.0 | 2.7 | 0.00 | 2.9 | 9.7 | 0.0 | -4.5 | 0.0 | 0 | 34 | 1 |
| 299 | 285 | 87 | 33 | 33 | 33 | 33 | 1 | 1 | 12.5 | 4.6 | 0.00 | 19.6 | 0.0 | 0.0 | -0.3 | 0.0 | 0 | 23 | 0 |
| 265* | 354 | 66 | 42 | 45 | 46 | 36 | 2 | 4 | 12.5 | -0.1 | 2.16 | 6.1 | 1.8 | 0.0 | 0.7 | 2.7 | 12 | 34 | 5 |
| 300 | 288 | 77 | 32 | 33 | 33 | 31 | 0 | 1 | 12.5 | 4.6 | 0.00 | 4.5 | 0.0 | 0.0 | -1.7 | 1.1 | 37 | 3 | 0 |
| 63 | 341 | 73 | 40 | 40 | 40 | 40 | 0 | 0 | 9.3 | 5.3 | 0.00 | 13.1 | 0.0 | 0.0 | -15.0 | 0.0 | 0 | 34 | 0 |
| 64 | 344 | 65 | 39 | 39 | 39 | 39 | 0 | 0 | 15.7 | 5.9 | 0.00 | 1.8 | 9.3 | 0.0 | 8.5 | 0.0 | 0 | 34 | 1 |
| 301 | 296 | 82 | 34 | 34 | 34 | 34 | 1 | 1 | 12.5 | 4.6 | 0.00 | 1.6 | 0.0 | 0.0 | -1.7 | 0.0 | 0 | 3 | 0 |
| 268 | 301 | 26 | 31 | 31 | 31 | 31 | 0 | 0 | 12.5 | 4.6 | 0.00 | 1.9 | 0.3 | 0.0 | 10.2 | 0.0 | 0 | 104 | 0 |
| 302 | 301 | 74 | 36 | 38 | 38 | 35 | 0 | 1 | 12.5 | 4.6 | 0.00 | 16.2 | 1.1 | 0.0 | -5.1 | 1.5 | 0 | 3 | 1 |
| 270 | 17 | 95 | 33 | 34 | 33 | 34 | 4 | 5 | 15.4 | 6.1 | 0.00 | 13.5 | 1.0 | 0.0 | 1.7 | 0.6 | 53 | 63 | 0 |
| 271 | 358 | 70 | 32 | 32 | 32 | 32 | 5 | 5 | 17.8 | 1.2 | 0.00 | 2.7 | 0.0 | 0.0 | -2.5 | 0.0 | 12 | 34 | 0 |

Table A4. ACDT Volume Scan Output for Volume Scan No. 4, Case Study No. 2
(Contd)

| | | | | | | | | | | | | | | | | | | | | | |
|-----|-----|-----|----|----|----|----|---|---|---|------|-----|------|-----|-----|-----|-------|-----|-------|-----|---|---|
| 303 | 310 | 51 | 31 | 31 | 31 | 31 | 0 | 0 | 0 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | 4.1 | 0.0 | 0105 | 0 | 1 | 1 |
| 304 | 310 | 56 | 36 | 36 | 36 | 36 | 1 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -3.8 | 0.0 | 0 | 3 | 0 | 1 |
| 372 | 21 | 52 | 37 | 37 | 37 | 37 | 1 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -3.8 | 1.4 | 16 | 63 | 0 | 3 |
| 373 | 1 | 54 | 38 | 38 | 38 | 38 | 0 | 0 | 0 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -0.5 | 0.0 | 12112 | 0 | 1 | 2 |
| 374 | 14 | 43 | 41 | 42 | 42 | 42 | 0 | 0 | 0 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | 2.4 | 0.0 | 42112 | 1 | 1 | 2 |
| 375 | 326 | 71 | 33 | 33 | 33 | 33 | 0 | 0 | 0 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -10.6 | 0.0 | 0 | 34 | 1 | 0 |
| 305 | 316 | 102 | 32 | 32 | 32 | 32 | 1 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -3.2 | 0.3 | 0 | 99 | 1 | 1 |
| 306 | 320 | 74 | 36 | 36 | 36 | 36 | 1 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -9.7 | 1.3 | 0 | 34 | 1 | 1 |
| 307 | 330 | 74 | 40 | 40 | 40 | 40 | 1 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -13.3 | 0.0 | 0 | 34 | 0 | 1 |
| 377 | 3 | 51 | 32 | 32 | 32 | 32 | 0 | 0 | 0 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | 0.0 | 0.0 | 0 | 112 | 1 | 0 |
| 378 | 4 | 56 | 36 | 36 | 36 | 36 | 0 | 0 | 0 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -7.0 | 0.0 | 54 | 67 | 0 | 1 |
| 379 | 43 | 71 | 37 | 40 | 40 | 40 | 0 | 0 | 0 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -0.9 | 5.0 | 0 | 116 | 1 | 5 |
| 380 | 271 | 48 | 38 | 38 | 38 | 38 | 1 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | 1.7 | 5.0 | 55100 | 5 | 3 | 2 |
| 381 | 308 | 77 | 44 | 44 | 44 | 44 | 1 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -8.7 | 2.2 | 0 | 34 | 1 | 1 |
| 92 | 7 | 47 | 39 | 39 | 39 | 39 | 0 | 0 | 0 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | 7.1 | 0.0 | 42112 | 1 | 0 | 1 |
| 383 | 348 | 66 | 33 | 33 | 33 | 33 | 0 | 0 | 0 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -6.6 | 0.0 | 0 | 34 | 1 | 0 |
| 308 | 336 | 101 | 36 | 36 | 36 | 36 | 1 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -3.1 | 0.0 | 0 | 107 | 0 | 1 |
| 309 | 340 | 101 | 38 | 38 | 38 | 38 | 1 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -4.9 | 0.0 | 0 | 107 | 0 | 1 |
| 310 | 341 | 107 | 35 | 35 | 35 | 35 | 1 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -3.6 | 0.0 | 0 | 106 | 0 | 1 |
| 311 | 343 | 94 | 31 | 31 | 31 | 31 | 1 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -4.6 | 0.0 | 0 | 109 | 0 | 1 |
| 312 | 346 | 111 | 32 | 32 | 32 | 32 | 1 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -7.6 | 0.0 | 0 | 108 | 0 | 1 |
| 313 | 314 | 62 | 32 | 32 | 32 | 32 | 0 | 0 | 0 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -1.6 | 5.7 | 39 | 34 | 0 | 2 |
| 313 | 349 | 61 | 31 | 31 | 31 | 31 | 1 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -4.7 | 0.0 | 0 | 110 | 0 | 1 |
| 314 | 359 | 124 | 41 | 41 | 41 | 41 | 1 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -5.5 | 0.1 | 0 | 90 | 1 | 1 |
| 315 | 29 | 85 | 34 | 34 | 34 | 34 | 1 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | 1.4 | 1.4 | 0 | 111 | 1 | 1 |
| 316 | 29 | 119 | 36 | 36 | 36 | 36 | 1 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -0.4 | 0.0 | 0 | 114 | 0 | 1 |
| 317 | 38 | 112 | 32 | 32 | 32 | 32 | 1 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | 0.8 | 0.2 | 0 | 115 | 1 | 1 |
| 318 | 241 | 212 | 39 | 41 | 41 | 41 | 4 | 4 | 4 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | 3.6 | 2.9 | 0 | 75 | 1 | 1 |
| 109 | 353 | 79 | 38 | 38 | 38 | 38 | 1 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | 0.8 | 0.3 | 22 | 34 | 0 | 2 |
| 320 | 48 | 141 | 32 | 32 | 32 | 32 | 3 | 3 | 3 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | 0.7 | 0.0 | 0 | 0 | 0 | 1 |
| 321 | 52 | 150 | 35 | 35 | 35 | 35 | 3 | 3 | 3 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | 1.8 | 0.0 | 0 | 67 | 0 | 1 |
| 322 | 102 | 31 | 39 | 41 | 41 | 41 | 0 | 0 | 0 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | 1.5 | 7.9 | 0 | 0 | 0 | 2 |
| 323 | 231 | 194 | 37 | 37 | 37 | 37 | 5 | 5 | 5 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | 2.9 | 0.0 | 0 | 0 | 0 | 1 |
| 324 | 236 | 157 | 32 | 32 | 32 | 32 | 4 | 4 | 4 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | 1.0 | 0.0 | 0 | 0 | 0 | 1 |
| 117 | 235 | 178 | 42 | 43 | 43 | 43 | 4 | 4 | 4 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | 1.1 | 0.0 | 0 | 0 | 0 | 1 |
| 118 | 307 | 21 | 33 | 33 | 33 | 33 | 1 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -10.5 | 0.0 | 0 | 3 | 0 | 1 |
| 119 | 285 | 68 | 34 | 36 | 36 | 36 | 1 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -0.9 | 3.7 | 37 | 3 | 0 | 2 |
| 325 | 254 | 140 | 42 | 45 | 45 | 45 | 3 | 3 | 3 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -0.1 | 1.3 | 50 | 97 | 1 | 2 |
| 326 | 265 | 102 | 33 | 33 | 33 | 33 | 2 | 2 | 2 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | 0.0 | 0.0 | 51 | 23 | 0 | 1 |
| 122 | 263 | 98 | 37 | 37 | 37 | 37 | 2 | 2 | 2 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | 1.6 | 0.0 | 51 | 23 | 0 | 1 |
| 327 | 289 | 71 | 32 | 32 | 32 | 32 | 1 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -3.9 | 0.0 | 37 | 3 | 0 | 1 |
| 328 | 276 | 47 | 33 | 36 | 36 | 36 | 0 | 2 | 3 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | 5.6 | 0.7 | 55102 | 1 | 5 | 1 |
| 329 | 38 | 116 | 31 | 31 | 31 | 31 | 4 | 4 | 4 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -0.1 | 0.0 | 0 | 0 | 0 | 1 |
| 126 | 349 | 71 | 38 | 42 | 42 | 42 | 0 | 3 | 7 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -1.2 | 4.0 | 22 | 34 | 2 | 4 |
| 129 | 12 | 93 | 38 | 38 | 38 | 38 | 1 | 1 | 1 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -5.1 | 0.2 | 0 | 63 | 2 | 0 |
| 131 | 331 | 80 | 37 | 41 | 41 | 41 | 0 | 1 | 4 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | 1.6 | 5.5 | 43 | 34 | 1 | 3 |
| 132 | 19 | 85 | 38 | 39 | 39 | 39 | 1 | 2 | 4 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -3.5 | 2.7 | 16 | 63 | 2 | 3 |
| 330 | 34 | 73 | 35 | 35 | 35 | 35 | 2 | 2 | 2 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | 3.2 | 0.0 | 0 | 116 | 0 | 1 |
| 331 | 54 | 154 | 32 | 32 | 32 | 32 | 8 | 8 | 8 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | 2.7 | 0.0 | 0 | 0 | 0 | 1 |
| 332 | 248 | 81 | 32 | 33 | 33 | 33 | 1 | 4 | 4 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -3.3 | 0.3 | 0 | 0 | 1 | 2 |
| 334 | 262 | 84 | 32 | 32 | 32 | 32 | 3 | 3 | 3 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | -7.9 | 0.0 | 0 | 0 | 1 | 1 |
| 335 | 278 | 62 | 33 | 35 | 35 | 35 | 2 | 3 | 4 | 12.5 | 4.6 | 0.00 | 2.1 | 7.9 | 0.0 | 4.2 | 0.2 | 56 | 0 | 0 | 1 |

Table A4. ACDT Volume Scan Output for Volume Scan No. 4, Case Study No. 2 (Cont'd)

| | | | | | | | | | | | | | | | | | | | | | | |
|------|-----|-----|----|----|----|----|---|---|---|------|------|------|------|-----|-----|-------|-----|-------|----|---|---|---|
| 139 | 18 | 79 | 47 | 47 | 47 | 47 | 0 | 0 | 0 | 12.7 | 4.5 | 0.00 | 7.1 | 0.0 | 1.0 | -9.7 | 0.0 | 57 | 63 | 0 | 1 | 2 |
| 334* | 312 | 34 | 34 | 35 | 35 | 32 | 2 | 3 | 5 | 12.5 | 4.5 | 1.75 | 2.4 | 5.7 | 0.0 | 1.9 | 5.1 | 58 | 0 | 3 | 5 | 1 |
| 337 | 329 | 70 | 32 | 32 | 32 | 30 | 1 | 3 | 3 | 12.5 | 4.5 | 0.00 | 0.5 | 0.0 | 0.0 | 5.4 | 0.0 | 0 | 0 | 0 | 1 | 1 |
| 338 | 334 | 72 | 33 | 33 | 32 | 33 | 3 | 4 | 4 | 12.5 | 4.5 | 0.00 | 2.4 | 0.0 | 0.0 | 3.3 | 0.5 | 43 | 34 | 0 | 2 | 1 |
| 339 | 344 | 75 | 32 | 32 | 32 | 32 | 1 | 3 | 3 | 12.5 | 4.5 | 0.00 | 0.2 | 1.3 | 0.0 | 1.4 | 1.5 | 0 | 0 | 0 | 1 | 1 |
| 340 | 356 | 36 | 36 | 32 | 32 | 32 | 4 | 4 | 6 | 12.5 | 4.5 | 0.00 | 3.3 | 1.1 | 0.0 | 2.5 | 2.9 | 0 | 34 | 2 | 4 | 1 |
| 341* | 7 | 55 | 40 | 41 | 41 | 40 | 0 | 3 | 4 | 12.5 | 4.5 | 0.00 | 3.4 | 1.2 | 0.0 | -1.5 | 1.1 | 59 | 0 | 5 | 2 | 1 |
| 342* | 14 | 50 | 42 | 46 | 46 | 46 | 2 | 4 | 4 | 12.5 | 4.5 | 0.00 | 0.5 | 1.2 | 0.0 | -0.2 | 1.0 | 0 | 0 | 2 | 2 | 1 |
| 343 | 19 | 96 | 34 | 34 | 34 | 34 | 4 | 4 | 4 | 12.5 | 4.5 | 0.00 | 1.9 | 1.3 | 0.0 | -0.3 | 0.3 | 53 | 63 | 1 | 1 | 1 |
| 344 | 29 | 94 | 32 | 32 | 32 | 32 | 4 | 4 | 4 | 12.5 | 4.5 | 0.00 | 0.0 | 0.0 | 0.0 | 1.1 | 0.2 | 0 | 0 | 0 | 1 | 1 |
| 345 | 34 | 71 | 32 | 33 | 33 | 32 | 3 | 4 | 4 | 12.5 | 4.5 | 0.00 | 3.3 | 0.0 | 0.0 | 0.4 | 1.0 | 0 | 0 | 0 | 2 | 1 |
| 346* | 0 | 62 | 45 | 46 | 46 | 45 | 0 | 4 | 5 | 12.5 | 4.5 | 0.00 | 3.5 | 1.5 | 0.0 | -4.5 | 2.0 | 13 | 34 | 5 | 4 | 1 |
| 152 | 237 | 178 | 40 | 40 | 40 | 40 | 4 | 4 | 4 | 12.1 | 4.5 | 0.00 | 5.5 | 2.3 | 0.0 | -9.5 | 0.0 | 0-16 | 1 | 0 | 2 | |
| 347 | 266 | 56 | 32 | 32 | 32 | 32 | 2 | 2 | 2 | 12.5 | 4.5 | 0.00 | 0.6 | 3.3 | 0.0 | -8.5 | 0.0 | 0 | 0 | 0 | 1 | 1 |
| 348 | 318 | 05 | 31 | 31 | 31 | 31 | 1 | 1 | 1 | 12.5 | 4.5 | 0.00 | 1.7 | 4.0 | 0.0 | 13.5 | 0.0 | 0 | 0 | 0 | 1 | 1 |
| 349 | 335 | 51 | 32 | 32 | 32 | 32 | 5 | 5 | 5 | 12.5 | 4.5 | 0.00 | 1.0 | 2.0 | 0.0 | 2.4 | 0.0 | 0 | 0 | 0 | 1 | 1 |
| 350 | 19 | 47 | 42 | 43 | 43 | 42 | 2 | 2 | 2 | 12.5 | 4.5 | 0.00 | 4.0 | 2.0 | 0.0 | -1.1 | 1.5 | 0 | 0 | 1 | 1 | 1 |
| 351 | 276 | 67 | 33 | 33 | 32 | 33 | 3 | 3 | 4 | 12.5 | 4.5 | 0.00 | 2.5 | 1.1 | 0.0 | 2.2 | 0.2 | 56 | 0 | 0 | 2 | 1 |
| 352 | 44 | 74 | 35 | 35 | 35 | 35 | 5 | 5 | 5 | 12.5 | 4.5 | 0.00 | 4.3 | 1.1 | 0.0 | -0.4 | 0.0 | 0116 | 0 | 1 | 1 | |
| 152 | 252 | 104 | 31 | 31 | 31 | 31 | 2 | 2 | 2 | 12.2 | -2.3 | 0.00 | 4.5 | 1.1 | 0.0 | 3.3 | 0.0 | 0 | 0 | 0 | 1 | 2 |
| 353 | 280 | 46 | 32 | 32 | 32 | 32 | 1 | 4 | 4 | 12.5 | 4.5 | 0.00 | 2.5 | 1.2 | 0.0 | 5.4 | 0.5 | 60102 | 0 | 3 | 1 | |
| 354 | 356 | 65 | 41 | 42 | 42 | 42 | 4 | 4 | 4 | 12.5 | 4.5 | 0.00 | 1.9 | 0.0 | 0.0 | 1.3 | 0.2 | 12 | 34 | 0 | 1 | 1 |
| 355 | 6 | 59 | 37 | 38 | 38 | 36 | 4 | 5 | 7 | 12.5 | 4.5 | 0.00 | 3.1 | 1.3 | 0.0 | -1.4 | 1.0 | 59 | 0 | 0 | 2 | 1 |
| 356 | 318 | 52 | 31 | 31 | 31 | 31 | 4 | 4 | 4 | 12.5 | 4.5 | 0.00 | 4.5 | 4.3 | 0.0 | -8.5 | 0.0 | 53 | 0 | 1 | 1 | 1 |
| 165 | 282 | 69 | 32 | 32 | 32 | 32 | 1 | 3 | 3 | 12.5 | 1.7 | 0.00 | 4.3 | 1.0 | 0.0 | -0.3 | 1.5 | 37 | 3 | 0 | 3 | 2 |
| 357 | 0 | 65 | 39 | 39 | 39 | 39 | 7 | 7 | 7 | 12.5 | 4.5 | 0.00 | 5.1 | 2.0 | 0.0 | -0.1 | 0.3 | 0 | 0 | 1 | 1 | 1 |
| 358 | 279 | 50 | 38 | 38 | 38 | 38 | 5 | 5 | 5 | 12.5 | 4.5 | 0.00 | 1.9 | 1.1 | 0.0 | 6.3 | 0.7 | 60108 | 0 | 1 | 1 | |
| 168 | 310 | 20 | 35 | 35 | 35 | 35 | 1 | 1 | 1 | 11.5 | -5.5 | 0.00 | 2.3 | 0.0 | 0.0 | -7.1 | 0.0 | 0 | -3 | 0 | 1 | 2 |
| 193 | 56 | 140 | 36 | 36 | 36 | 36 | 2 | 2 | 2 | 12.5 | 10.5 | 0.00 | 5.3 | 1.7 | 0.0 | -2.5 | 1.2 | 0 | 67 | 2 | 0 | 2 |
| 194 | 304 | 69 | 31 | 31 | 31 | 31 | 0 | 0 | 0 | 14.0 | -5.4 | 0.00 | 2.1 | 1.2 | 0.0 | -6.3 | 0.0 | 0 | 3 | 1 | 0 | 2 |
| 192 | 279 | 91 | 38 | 38 | 38 | 38 | 1 | 1 | 1 | 12.7 | -1.5 | 0.00 | 5.0 | 0.0 | 0.0 | -0.2 | 0.0 | 0 | 0 | 0 | 1 | 2 |
| 199 | 232 | 205 | 45 | 45 | 45 | 45 | 5 | 5 | 5 | 7.1 | 7.2 | 0.00 | 4.3 | 0.0 | 0.0 | -1.7 | 0.0 | 38 | 16 | 0 | 1 | 2 |
| 203 | 341 | 76 | 40 | 40 | 40 | 40 | 0 | 0 | 0 | 17.1 | 11.5 | 0.00 | 0.5 | 1.3 | 0.0 | -13.6 | 0.1 | 0 | 34 | 1 | 1 | 2 |
| 206 | 343 | 81 | 32 | 32 | 32 | 32 | 0 | 0 | 0 | 13.0 | 0.3 | 0.00 | 5.1 | 1.2 | 0.0 | -7.6 | 0.2 | 0 | 34 | 1 | 1 | 2 |
| 207 | 351 | 78 | 35 | 35 | 36 | 32 | 0 | 3 | 6 | 11.9 | 0.7 | 0.00 | 4.7 | 1.3 | 0.0 | -4.0 | 4.9 | 22 | 34 | 2 | 5 | 1 |
| 211 | 324 | 84 | 34 | 34 | 34 | 34 | 1 | 1 | 1 | 11.5 | 0.5 | 0.00 | 0.6 | 1.2 | 0.0 | -9.1 | 0.0 | 43 | 34 | 1 | 0 | 2 |
| 213 | 19 | 99 | 33 | 33 | 33 | 33 | 4 | 4 | 5 | 12.5 | 5.5 | 0.00 | 2.3 | 1.1 | 0.0 | -1.1 | 1.2 | 16 | 63 | 1 | 2 | 2 |
| 215 | 312 | 61 | 32 | 32 | 32 | 31 | 0 | 1 | 3 | 15.4 | 0.1 | 0.00 | 4.5 | 1.3 | 0.0 | -7.2 | 2.1 | 39 | 34 | 1 | 2 | 2 |
| 216 | 24 | 84 | 39 | 39 | 39 | 39 | 4 | 4 | 4 | 14.5 | 4.7 | 0.00 | 1.8 | 1.1 | 0.0 | -3.0 | 0.2 | 54 | 63 | 1 | 1 | 2 |
| 219 | 357 | 53 | 46 | 46 | 46 | 46 | 0 | 1 | 2 | 13.5 | 10.7 | 0.00 | 3.6 | 1.7 | 0.0 | -0.1 | 2.7 | 12 | 34 | 1 | 2 | 2 |
| 224 | 351 | 65 | 39 | 39 | 39 | 39 | 2 | 0 | 2 | 11.9 | -0.1 | 0.00 | 1.9 | 1.4 | 0.0 | -0.3 | 0.0 | 61-34 | 1 | 0 | 2 | |
| 227 | 351 | 60 | 42 | 42 | 42 | 42 | 0 | 0 | 0 | 14.3 | 5.0 | 0.00 | 13.5 | 5.3 | 0.0 | 7.9 | 0.7 | 61 | 34 | 1 | 1 | 2 |

Table A4. ACDT Volume Scan Output for Volume Scan No. 1, Case Study No. 2 (Cont'd)

| CLUSTER OUTPUT | | | | | | | | | | | | | | | | | | | |
|----------------|------|------|-------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| CENTROID | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | | 8 | | 9 | | 10 | |
| TRK | AZM | RNG | AV | PA | V | A | S | AN | DEP | VEL | DIR | VEL | DIR | VEL | DIR | VEL | DIR | VEL | DIR |
| 40 | 080 | AM | 05 | 08 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 47 | 55 | 147 | 45 | 48 | 1 | 1.4 | 14.4 | 14.4 | 14.4 | 14.4 | 14.4 | 14.4 | 14.4 | 14.4 | 14.4 | 14.4 | 14.4 | 14.4 | 14.4 |
| 37 | 087 | 70 | 33 | 33 | 1 | 1.4 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 |
| 48 | 299 | 61 | 13 | 13 | 1 | 1.4 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 |
| 38 | 230 | 007 | 45 | 45 | 1 | 1.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 49 | 237 | 156 | 44 | 44 | 1 | 1.4 | 1.6 | 1.6 | 1.6 | 1.6 | 1.6 | 1.6 | 1.6 | 1.6 | 1.6 | 1.6 | 1.6 | 1.6 | 1.6 |
| 39 | 313 | 63 | 34 | 37 | 1 | 1.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 |
| 50 | 255 | 142 | 61 | 65 | 1 | 1.4 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| 51 | 264 | 100 | 34 | 37 | 1 | 1.5 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| 52 | 293 | 91 | 31 | 31 | 1 | 1.4 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 |
| 12 | 358 | 60 | 42 | 42 | 1 | 1.1 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| 53 | 18 | 96 | 33 | 34 | 1 | 1.4 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 |
| 16 | 20 | 85 | 36 | 39 | 1 | 1.4 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 |
| 46 | 10 | 45 | 40 | 40 | 1 | 1.4 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 |
| 54 | 24 | 85 | 37 | 39 | 1 | 1.4 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 |
| 55 | 273 | 41 | 33 | 36 | 1 | 1.4 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 |
| 22 | 351 | 76 | 37 | 40 | 1 | 1.4 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 |
| 43 | 334 | 81 | 35 | 41 | 1 | 1.4 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 |
| 56 | 277 | 64 | 33 | 35 | 1 | 1.4 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 |
| 57 | 11 | 73 | 47 | 47 | 1 | 1.4 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 |
| 53 | 318 | 53 | 32 | 35 | 1 | 1.4 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 |
| 59 | 6 | 57 | 39 | 41 | 1 | 1.4 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 |
| 60 | 200 | 48 | 36 | 38 | 1 | 1.4 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 |
| 61 | 351 | 62 | 41 | 43 | 1 | 1.4 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 |
| OVER | | | | | | | | | | | | | | | | | | | |
| VOL | HHMM | AREA | WFLUX | NEAR | NEAR | NEAR | NEAR | NEAR | NEAR | NEAR | NEAR | NEAR | NEAR | NEAR | NEAR | NEAR | NEAR | NEAR | NEAR |
| SCAN | | KKM2 | KYT/H | CELL | CLST | CCAT | VOL | IS | FL | LM/S | AN/S | NO | CTR | CTR | CTR | CTR | CTR | CTR | CTR |
| 4 | 1551 | 5.2 | 31.29 | 6.6 | 17.0 | 0.0 | 140 | 24 | 10 | 10.0 | 5.1 | 358 | 67 | 116 | C | C | C | C | C |